

Changes of Forest Stands Vulnerability to Future Wind Damage Resulting from Different Management Methods

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Abstract: The structure of forests stands changes continuously as a result of forest growth and both natural and anthropogenic disturbances like windthrow or management activities – planting/cutting of trees. These structure changes can stabilize or destabilize forest stands in terms of their resistance to wind damage. The driving force behind the damage is the climate, but the magnitude and sign of resulting effect depend on tree species, management method and soil conditions. The projected increasing frequency of weather extremes in the whole and severe storms in particular might produce wide area damage in European forest ecosystems during the 21st century. To assess the possible wind damage and stabilization/destabilization effects of forest management a number of numeric experiments are carried out for the region of Solling, Germany. The coupled small-scale process-based model combining Brook90 [1] and SCALAr DIStribuiton turbulence model [2-4] is implemented. The SRES climate scenarios A1B and B1 dynamically downscaled by Climate Local Model CLM [5] are used to project the future climate conditions in the area. The experiments are performed for two tree species (spruce and beech) and a mixed stand and for two target diameter harvesting scenarios. The results show considerable increment of wind damage risks towards 2100 compared to “present climate conditions”, caused by the combination of weak increase of wind speed and precipitation and strong increase of air and soil temperature. The effect is stronger for coniferous species than for deciduous ones. It is shown that management activities have a strong destabilizing effect on forests due to joint influence of climatic factors and decrease of stand density.

Keywords: Wind damage, target diameter harvesting, climate change, SCADIS, Brook90, coupled model.

INTRODUCTION

The structure of forests stands changes continuously as a result of forest growth or abruptly due to both natural and anthropogenic disturbances like windthrow or stem break or forest management activities – planting/cutting of trees. These structure changes can stabilize or destabilize forest stands in terms of their resistance to wind damage and increase or decrease the wind load on trees in a forest. The result would be the higher or lower probability of subsequent wind damage [6, 7].

By evaluating the consequences of natural impacts on forest structure [8] found out that after a windthrow or clear-cut the risks increase strongly for the remaining stand around the gap. The studies of [6, 9] showed that any kind of forest thinning or harvesting results in instant destabilizing of remaining stand. In present study the attempt is made to consider the changes in climatic factors other than wind speed and soil temperature and to assess the long-term consequences of forest management activities. One of the standard silvicultural methods is the uneven-aged natural regeneration through selective thinning, which is assumed to

yield important ecological benefits [10]. It is ecologically and economically worthwhile to harvest older trees with a gross dimension [11]. This way the forests could store higher amounts of carbon and develop more quality timber. In selection harvest systems, individual trees or small groups of trees are harvested at periodic intervals. The selection is primarily based on their physical condition or degree of maturity [12]. Also the target diameter harvesting regime leads away from whole clearcut areas as a method of final harvesting when individual trees have reached a certain diameter rather than when stands have reached rotation age [13]. So the harvesting results in a forest without large gaps but with less density, decreased averaged height, diameter at breast height (DBH), leaf area index (LAI) and vertical distribution of leaf area density (LAD).

The driving force behind the forest damages dynamics is the climate impact; however the magnitude and sign of resulting effect depend on tree species, management method and soil conditions. The projected increasing frequency of severe storms might produce wide area damage in European forest ecosystems during the 21st century [14-18]. It was pointed out that forest management using adequate decision support systems (DSS) can considerably reduce the risk of damages [19]. The DSS “Forest and Climate Change” which is currently being developed at the Göttingen University [20] is aimed to provide a tool for the quantitative assessment of biotic and abiotic risks of forest ecosystems under the

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Table 1. Stand Characteristics and Model Parameters for Different Harvest Intensities of Norway Spruce and European Beech. The Sources of Data are Given in [32]

Parameter	Unit	Norway Spruce			European Beech		
Variante		sp1	sp2	sp3	be1	be2	be3
age	years	90	90	90	120	120	120
stand density	tree ha ⁻¹	371	294	222	202	171	131
tree height	m	27.5	26.8	26.1	30.3	30.2	29.3
DBH	cm	38.6	35.8	33.4	44.6	43.9	40.0
solid volume	m ³ _(s) ha ⁻¹	519	351	228	486	395	243
max leaf are index	m ² m ⁻²	6.6	4.6	3.1	7.2	5.1	3.4
relative winter LAI	[-]	0.8	0.8	0.8	0.15	0.22	0.32
stem area index (SAI)	m ² m ⁻²	1.40	0.96	0.63	0.55	0.45	0.29

conditions of changing climate. An improved understanding of damages is essential for addressing the environmental and policy implications of climate variability and global change. Therefore the objective of this study is to assess the spatio-temporal variability of the effect which different target diameter harvesting (TDH) regimes excersize on wind damage risks for two typical for Germany tree species (spruce and beech) on different soil types under the projected future climatic conditions.

MATERIALS AND METHODOLOGY

Investigation Area and Tree Species

The Solling area belongs to German Highlands covering the sub-montane and the montane zone up to 550 m a.s.l. The area chosen for the study is located between 51.5°N and 52.1°N and between 9.3°E to 9.9°E, i.e. about 3600 km² is chosen for the investigation. The area belongs to the suboceanic climate with strong orographic effect on both temperature and precipitation. For the period 1950-2000 T_a in the investigation area was between 6.5°C and 9°C, the mean annual precipitation between 600 mm and about 1000 mm [21]. The measurement data show [22] that during the period 1969-2002 the decadal mean values of both T_a and annual precipitation sums have an increasing tendency in Solling area. While the temperature increases both in summer and in winter, the increase of annual precipitation is caused mainly by the raise of winter precipitation. The mean annual precipitation sum for the mentioned period was 1095 mm while for the last decade (1190-2002) it reached 1193 mm.

The soils on sandstones and pure sand sediments are generally very acid nutrient poor dystic cambisols [23] and on loess-dominated sites eutric cambisols and haplic luvisols. The forest covers about 42% of the study area, with the share of deciduous about 26%, coniferous - 11% and with 5% of mixed forests (Fig. 1). Fig. (1) shows the spatial distribution of the land-use classes in the study area based on the Corine Land Cover 2000 dataset.

Forest Management Scenarios

In order to study the influence of stand structure changes caused by forest management activities on stand resistance to wind damage two scenarios of TDH and a reference

unmanaged stand are simulated. The calculations of all scenarios were performed for pure stands of both species - spruce and beech - and for a mixed stand. As reference unmanaged stands for beech (be1) and spruce (sp1) we use mature stands of the second yield class [24] with a DBH correction according to [25]. In the second variant of beech (be2) all trees with DBH ≥ 60 cm are harvested. In the third (be3), the target diameter for harvesting was set on 50 cm. The two different utilisation scenarios for spruce are on 45 cm (sp2) and on 40 cm (sp3). The diameter distribution and the effects of these harvesting scenarios on the mean stand characteristics are modeled with the forest simulator BWInPro7 [26]. The resulting stand parameters are summarized in Table 1. To simulate the risks for mixed stands with equal shares of beech and spruce the simulations were carried out for pure spruce and beech stands separately and the resulting risks were averaged with correspondent (in this case - equal) shares [27].

Climate Scenarios

To represent the possible future climatic conditions, the modeling results of two Special Report on Climate Scenarios (SRES) climate projections A1B and B1 for the period of 2001-2100 as well as 20th century scenario C20 for the period of 1960-2000 are used as defined in German framework program "klimazwei". The calculations done by coupled general circulation model - ocean model, ECHAM5-MPIOM, and dynamically downscaled using Climate Local Model, CLM [28] to a spatial resolution of 0.2°×0.2° (two runs per scenario) are obtained from CERA data base [29]. For all variables the time series of runs 1 and 2 of A1B and B1 are merged with correspondent runs of C20 so that continuous time series from 1960 to 2100 are built for both runs of A1B and B1. The calculations of wind damage risks with CLM data have been carried out according to the recommendations of [30]. Spatial averaging over the 9 CLM grid points to represent the study area is carried out for all climate characteristics. The calculations of abiotic risks have been done with daily resolution, separately with runs 1 and 2 for both merged C20-A1B and C20-B1. The results for each run are aggregated to annual means. To describe the tendencies of climate development the spatial mean values are then averaged over the 30-years periods: 1981-2010 (P0) – assumed as "actual state" or "reference period", 2011-2040 (P1), 2041-2070 (P2) and 2071-

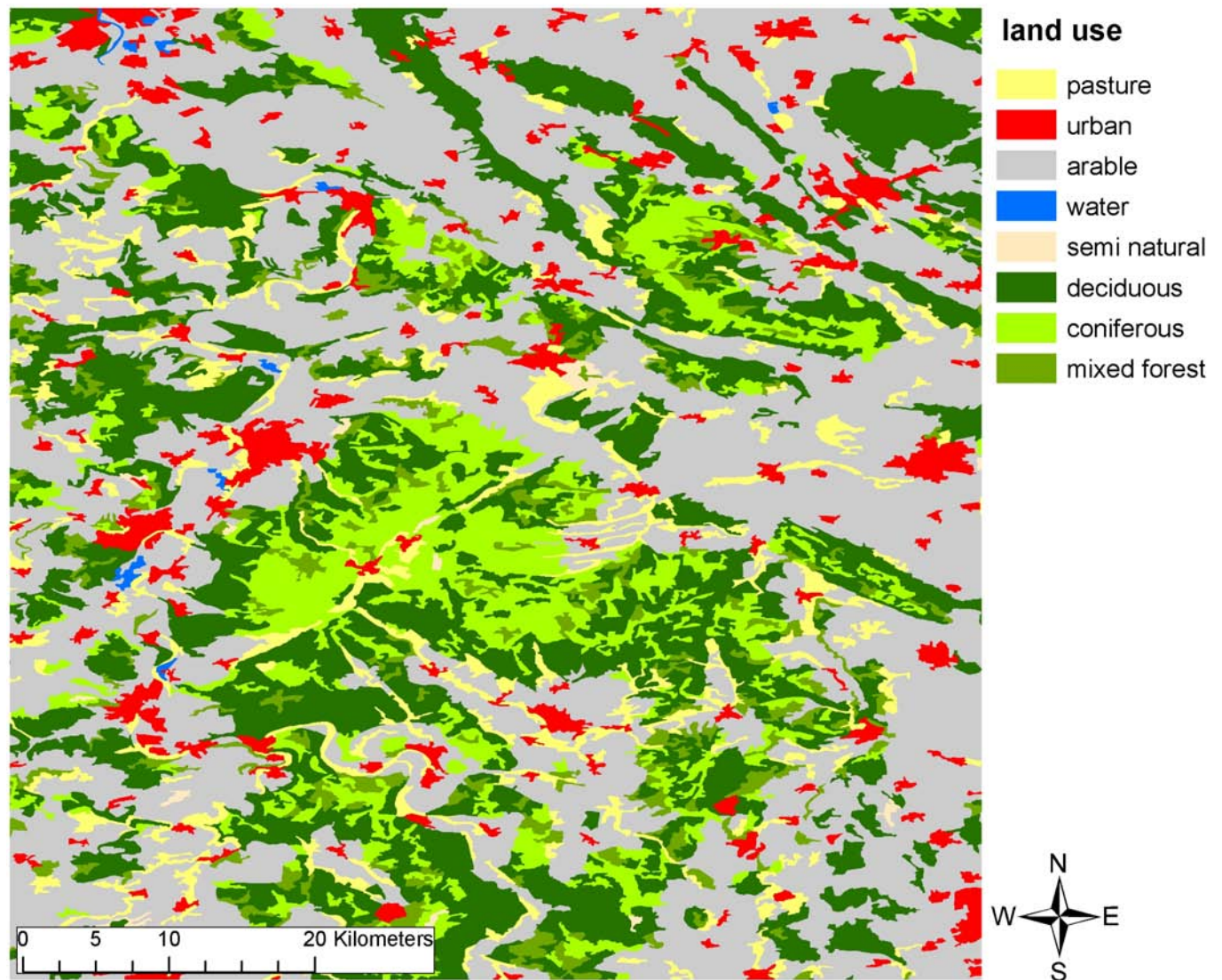


Fig. (1). Map of Solling site showing the different land use based on CORINE Land Cover 2000; Umweltbundesamt, DLR-DFD 2004.

2100 (P3) and relative differences are calculated: $\Delta\varphi_i = (\varphi_i - \varphi_0) / \varphi_0 * 100\%$, where φ_i is the 30-years mean value of the spatially averaged climate variable listed above for the climatic period $i = 0, 1, 2, 3$.

Soil and Root Parameters

For the spatially distributed simulation we used the digital soil map of Germany at a scale of 1:1000000 [31] and the digital metadata corresponding to the mentioned soil map. This map is subdivided accordingly to the main land cover types (forest, cropland and grassland).

The architecture of root systems is influenced by species and age of trees, soil properties, the depth of ground water and thus, indirectly by climate conditions. The detailed description of soil and root modeling approach is given in [32].

Preprocessing of GIS Coverage's and Input Datasets

To combine the spatial information the joint “look up table” is created with the unique attributes for each coverage within the model area. The first step has been to construct this table in ArcGis (Version 9.2; ESRI inc., Redlands, CA),

which is the unique superposition of the climate, soil and land-use GIS-data layers. In the second step the constructed dataset is used for the initialization of the model runs. The simulations are run for forest sites only.

Models Description (BROOK 90)

To simulate the water balance of forest stands in this paper we use the BROOK90 (Version 4.4e) - a 1D-Soil-Vegetation-Atmosphere Transfer (SVAT) Model [33-35]. BROOK90 has been developed to be applicable to different and changing land use. It simulates interception by a single layered stand, evapotranspiration, soil water and a streamflow consisting of surface runoff, bypass flow, down slope flow and base flow. The soil water transport is simulated with the Darcy-Richard equation. BROOK90 is a detailed, process-oriented model that can be used to study the soil water budget of forest stands over a broad set of study sites (e.g. [36-40]).

Models Description (SCADIS)

The atmospheric boundary-layer model SCADIS [2, 4] based on E- ω scheme (where E is turbulent kinetic energy

and ω is the specific dissipation of E) was used. The two-equation closure approach does not require a predefined mixing length and is thus naturally suited to modeling atmospheric flows over heterogeneous surfaces. Modification of model constants implemented in the model according to [3] extends the generality and applicability of approach to inhomogeneous canopy flow. This modification was found robust and performed well for wide range of canopies. To be driven the canopy flow model requires minimal set of tractable parameters describing canopy properties such as LAD and aerodynamic drag coefficient C_d . Model equations and details about numerical schemes and boundary conditions can be found in above mentioned papers.

Critical Wind Speed (CWS) and Risk Assessment

The CWS for windbreak, CWS_{break} , and for overturning, CWS_{ot} , defined as the speed at the tree tops, are calculated as in ForestGALES. The detailed description and discussions of the approach are given in [19, 41]. Here the main equations are shown:

$$CWS_{break} = \frac{1}{\kappa D} \left[\frac{\pi MOR * DBH^3 f_{knot}}{32 \rho G (d-1.3) f_{CW}} \right]^{\frac{1}{2}} * \ln \left(\frac{h-d}{z_0} \right) \quad (1)$$

$$CWS_{ot} = \frac{1}{\kappa D} \left[\frac{C_{reg} * SW f_{knot}}{32 \rho G d f_{CW}} \right]^{\frac{1}{2}} \ln \left(\frac{h-d}{z_0} \right) \quad (2)$$

where $\kappa = 0.41$ is von Karman's constant, $d(m)$ is the zero-plane displacement, $z_0(m)$ is the aerodynamic roughness, $D(m)$ is the average spacing between trees, DBH (m) is diameter at breast height (1.3 m above ground), $h(m)$ is mean tree height (Table 1) and ρ (1.226 kg m^{-3}) is the dry air density. C_{reg} (N m kg^{-1}) is a regression constant that is dependent on soil and rooting depth and SW (kg) is the stem weight of the tree. The factors f_{knot} ($= 0.85$) and f_{CW} ($= 1.17$) account for the reduction in wood strength due to knots and the additional load due to the overhanging weight of the tree displaced from the vertical position by the wind stress. The f_{edge} , taking into account the position of the tree relatively to the forest edge is ignored because of the assumption of horizontal homogeneity. G is a dimensionless gust factor [9, 41]:

$$G = 18.585 - 28.35 \cdot \frac{D}{h} + 1.59165 \cdot \ln \left(\frac{D}{h} \right) \quad (3)$$

Influence of rooting depth was taken into account. We assume that the tree anchorage and consequently the CWS estimated by means of functions based on tree pulling experiments are valid for "average" species-specific effective rooting depths: 0.91 m for spruce and 1.3 m for beech. Then the deviations of rooting depths from these mean values caused by combination of tree species and soil type [42] produce a correspondent linear positive or negative deviations from mean tree anchorage [43-45] and, thus, deviations of CWS from the initial "average" value.

In general, the risk of windthrow increases with increasing soil moisture content because of the weakening of tree anchorage and consequent reduction of CWS [46]. As a dynamic indicator of the soil moisture status, we use the time-dependent relative extractable soil water, $REW(t)$, which is calculated with the daily timestep as the ratio of actual to maximum extractable water according to [47]:

$$REW(t) = \frac{\theta_v(t) - \theta_R}{\theta_{fc} - \theta_R} \quad (4)$$

where θ_v [$\text{m}^3 \text{ m}^{-3}$] is the actual (correspondingly – daily) volumetric (subscript "v") soil water fraction; θ_{fc} ($\text{m}^3 \text{ m}^{-3}$) is the maximum soil water content extractable by plants (subscript "fc" means field capacity), and θ_R ($\text{m}^3 \text{ m}^{-3}$) the residual soil water content. We distinguish between dry and wet soil conditions where the wet conditions mean that the soil moisture has exceeded a certain threshold and the tree anchorage starts to decrease. As there are no published data on the critical level of soil moisture, the threshold of $REW(t) \geq 0.6$ is chosen in this study because at this level the optimum water content has been exceeded [48, 49]. The rate of mineralization, used as a proxy, slows down which indicates the prevailing anaerobic conditions and consequently filling the most soil pores with water. The moistening of the soil beneath a soil-root plate reduces the trees resistance to wind [50]. Therefore, we assumed for free draining soils that when $REW(t)$ exceeds 0.6 the CWS decreases linearly:

$$CWS(t) = \begin{cases} \frac{CWS_{ot} * 0.6}{REW(t)}; & REW(t) \geq 0.6 \\ CWS_{break}; & REW(t) < 0.6 \end{cases} \quad (5)$$

The risks are quantified as a share of damaged vegetation in total stand ($0 \leq SH \leq 1$) which is a function of wind load. The minimal speed leading to windthrow is $CWS_{min} = 8 \text{ m s}^{-1}$ (correspondent load is denoted as F_{Vmin}) and the wind speed of $CWS_{abs,max} = 40 \text{ m s}^{-1}$ is set as the load of full damage, i.e. all trees in stand are damaged [51] (correspondent load is denoted as $F_{Vabs,max}$). The relative load provided by actual wind is then:

$$F_{act} = 1 - \frac{F_{Vabs,max} - F_{Vact}}{F_{Vabs,max} - F_{Vmin}} \quad \text{and} \quad (6)$$

$$SH = 1 - F_{act}^b, F_{Vact} \geq F_{Vmin} \quad (7)$$

where $b = 3.73$ is the best approximation of damage curves for unmanaged stand presented by [51]. To assess the effects of forest structure changes resulting from windthrow events on the probability of next damage event the calculations are carried out in two ways. First – the damage is summed up during the 30-years period, but the forest structure does not change. Second – the damage is summed up and the damaged trees are "removed" from the stand – accordingly the stand density and LAI decrease. The calculations with BROOK90 continue from the time point of damage with the new values of structural characteristics. The stand's microclimate changes which in turn enhances or inhibits the

following windthrow events thus creating positive or negative feedbacks.

Initial and Boundary Conditions

The simulation period started on the 1.1.1960, whereby the evaluations were accomplished for the following four periods: P0: 1981-2010, P1: 2011-2040, P2: 2041-2070, P3: 2071-2100. The period 1960-1980 is used as an initialization run. Due to the long initialization time from 1960 to the first analysis period the soil profiles were assumed to be saturated at the beginning, with an initial matrix potential of -10kPa for all locations and horizons. To reach a maximum of simulation speed, the partial differential equations were solved with a maximum of 20 iterations per day. The minimum allowed iteration time step for BROOK90 is “2” [1]. The maximum change in soil wetness or saturation fraction for any layer in iteration was set to 0.5 %. For all locations at the bottom of the soil (2 m) free drainage was accepted.

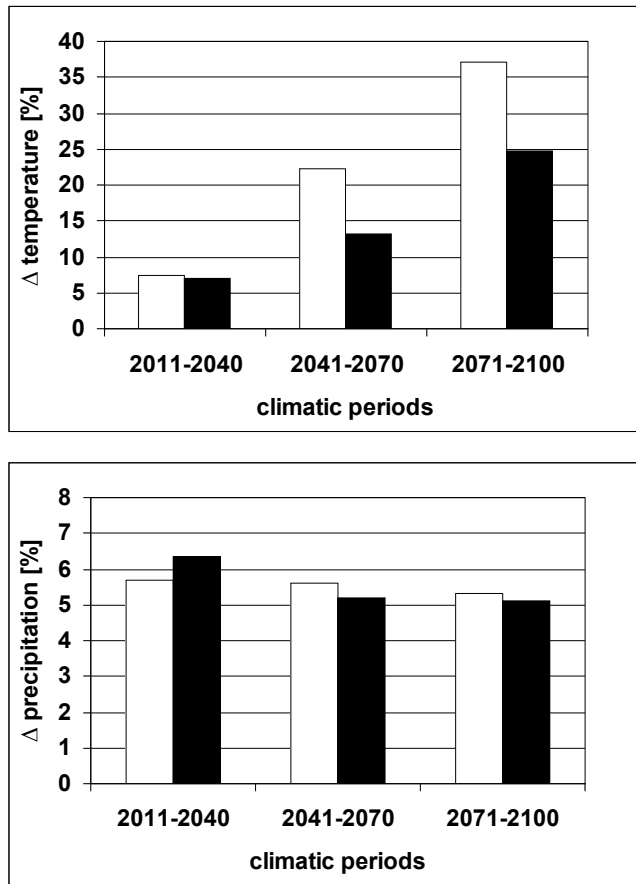


Fig. (2). The changes of annual mean values of air temperature (upper panel) and precipitation (lower panel) averaged over 30-years climatic periods relatively to the reference period (P0= 1981-2011) for two SRES scenarios: □: A1B and ■: B1.

RESULTS AND DISCUSSION

Climate Conditions

To characterize the projected climate conditions in 21st century in Solling area the CLM-data were post-processed according to the recommendations of [30]. The data of A1B_1, A1B_2, B1_1 and B1_2 are aggregated to annual

means (sums in case of precipitation). Spatial averaging over the 9 CLM grid points is carried out for all mentioned climate characteristics in order to represent the study area.

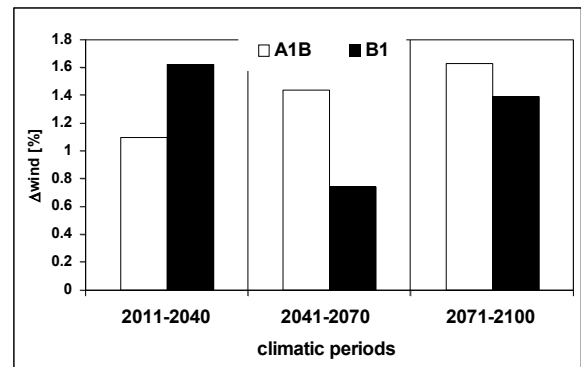


Fig. (3). The changes of annual mean values windspeed averaged over 30-years climatic periods relatively to the reference period (P0= 1981-2011) for two SRES scenarios: □: A1B and ■: B1.

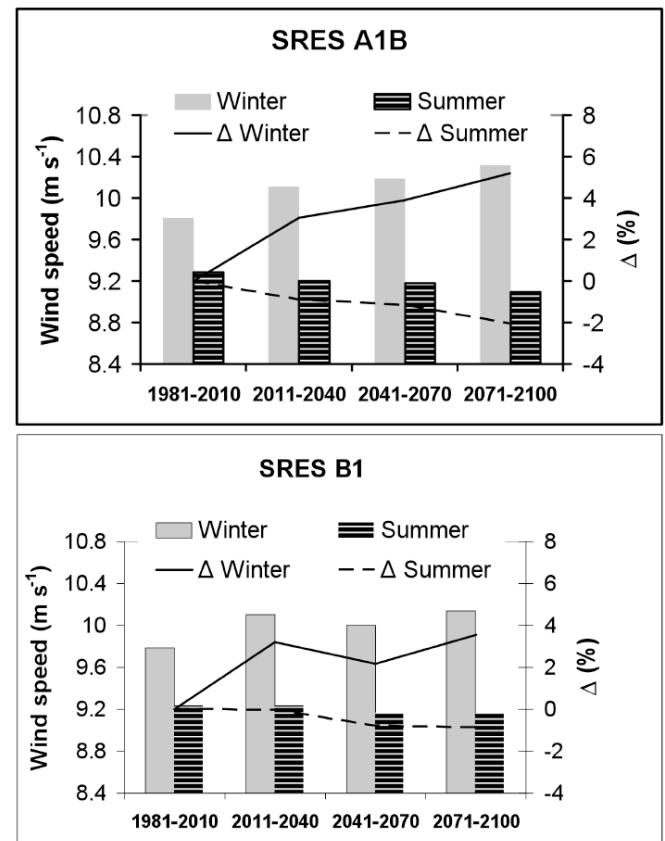


Fig. (4). The changes of seasonal mean values of windspeed averaged over 30-years climatic periods absolute values and relative to the reference period (P0= 1981-2011) for two SRES scenarios: A1B (upper panel) and B1 (low panel). The vertical bars indicate the wind speed (left Y-axis); the lines indicate the relative changes, Δ (right Y-axis).

The spatial variations within the chosen area are very low so that the spatial means are assumed to be representative. To describe the tendencies of climate development the spatial mean values of meteorological variables are averaged over the 30-years periods: P0-P3 and relative differences are calculated as described above in subsection “climate scenarios”. The analysis of climate scenarios data shows

(Fig. 2) for both scenarios an increase of precipitation to $\Delta P_1 \approx 6\%$ and then slight monotonical decrease towards 2100 to $\Delta P_3 \approx 5\%$. However, the air and soil temperatures increase monotonically and rather strongly towards P3 with $\Delta T_3 > 37\%$ in A1B and $\Delta T_3 > 24\%$ in B1.

In both scenarios the daily mean (V_{av}) (Fig. 3) and maximal wind velocity (V_{max}) (not shown) do not change strongly during 21st century. In A1B both V_{av} and V_{max} increase continuously towards P3 with $\Delta V_{av,3}$ going up to 2.3% and $\Delta V_{max,3}$ up to 1.6%. In B1 the strongest increases – 1.6% for ΔV_{max} and 2.2% for ΔV_{av} occur from P0 to P1 exceeding the correspondent ΔV_{max} and ΔV_{av} values for A1B. They decrease to P2 and increase slightly again in P3. Fig. (4) shows that the tendencies of annual mean wind speed are mainly caused by the pattern of mean winter windspeed. The mean wind in summer decreases monotonically with changes up to 2% under A1B and less than 1% under B1. That compensates partially the rather high increases of mean wind in winter – up to 6% (P3) under A1B and up to 4% (P3) under B1.

Model Results and Discussion

To analyse the impact of TDH on spatial and temporal pattern of windthrow risk the calculations are carried out separately for separate runs: A1B_1, A1B_2, B1_1 and B1_2 and then aggregated to 30-years-period means. Finally the soil and forest type distributions are superimposed with climate data and the damage risks are calculated. The results are the absolute differences between damaged share of trees in stands during the reference period (P0) and climate periods (P1-P3) for spruce and beech stands managed by different TDH (sp2, sp3, be2, be3).

Fig. (5) shows that in average in the investigated area the future changes in climate conditions will result in a very weak increase of wind damage from about 3% in P0 to approximately 5% in P3. The magnitudes of changes are very similar for both scenarios. It is however clearly visible that the climatic factor which controls the changes of wind risks is the wind speed - the temporal course of damages follows the pattern of changes in the windspeed (Figs. 3, 4). While the increase of windspeed and wind damage under A1B is weak but monotonical, the changes under B1 are also weak but experience a slight decrease between P1 and P2 caused by decrease of changes in wind speed and by winter mean in particular (Fig. 4).

The changes from P0 to P1 are stronger for B1 because of stronger increase in windspeed and precipitation in this period.

Figs. (6, 7) demonstrate that within the investigated area the damage risks vary considerably from almost no damage to more than 40% so that the area-averaged estimation should be used with care. However, it is demonstrated that the spatial patterns of damage under A1B and B1 are very similar and correspond to the distribution of forest types (Fig. 1). Considering the climate development in 21st century one can see that the damage risks increase towards 2100 both under A1B and B1 conditions. The spatial pattern of risks does not undergo any notable changes so that the “hot spots” of high damage remain on same places, but increase in magnitudes. Considering the influence of the harvesting

regime one can see that the forest management has generally an immediate destabilizing effect on forest ecosystems which was also concluded by [6]. The harvesting of highest trees in a stand results in a decreasing of mean stand height and thus should contribute to the stand stabilization. However, the increasing of mean distance between trees which is one of the key variables influencing the CWS results in the strong decreasing of the CWS and thus to stand's destabilization. On the other hand the reduced tree cover and LAI results in the complicated interactions of location- and species-dependent factors leading to decrease or increase of soil water content [7]. This respectively can lead to stabilizing or destabilizing of forest stands. Figs. (6, 7) show that under both A1B and B1 scenarios and under the conditions of Solling the TDH variants sp2,3 and be2,3 invariably lead to the destabilization for both species and all locations (soils). The magnitude of TDH contribution to the destabilization of stands remains almost constant towards 2100. It indicates that the contribution of the stand density to destabilization is higher than of the increase of soil water content. Comparing the spatial patterns of damage in unmanaged stand, sp1, be1 to sp2, 3 and be2, 3 one can see that while the damage pattern in managed stands is similar to the unmanaged ones, the patterns of intensity increments differ for different TDH regimes. The reasons are the different magnitudes of destabilisation for beech (lower) and spruce (higher effect). On example of unmanaged stand in reference period P0 the Fig. (8) shows the spatial distribution of wind damage risks superimposed on forest types. One can clearly see that the highest damage – up to 17% occurs in coniferous stands. Most of the beech stands remain within the range of 2.5% with the “hot spot” – up to 5%. In the mixed stand the damage risks are consequently within the range of 10%. Thus the beech stands have generally lower risks than spruce in spite of the lower stand density. The reason is that other factors such as: lower mean stand height, deeper rooting and lower slenderness (h/DBH ratio) provide higher stabilizing effect for beech stands compared to spruce.

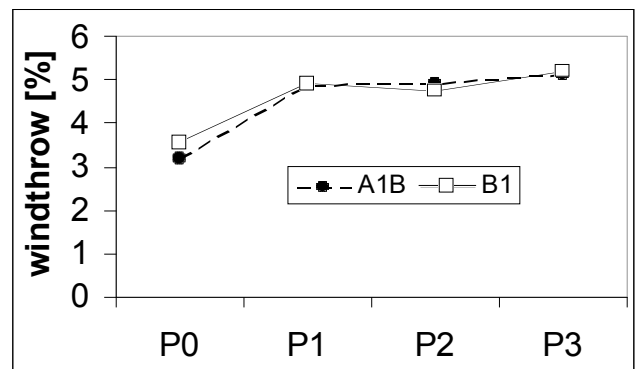


Fig. (5). The changes of area-averaged 30-years mean values of windthrow damage in Solling area for two SRES scenarios: A1B and B1.

The averaged over species stand damage (Fig. 9) shows that under both climate scenarios the damage risks for spruce increase monotonously towards 2100. The temporal course of risks for beech stands is completely different. The risks increase slightly from P0 to P1 and then decrease continuously toward P3.

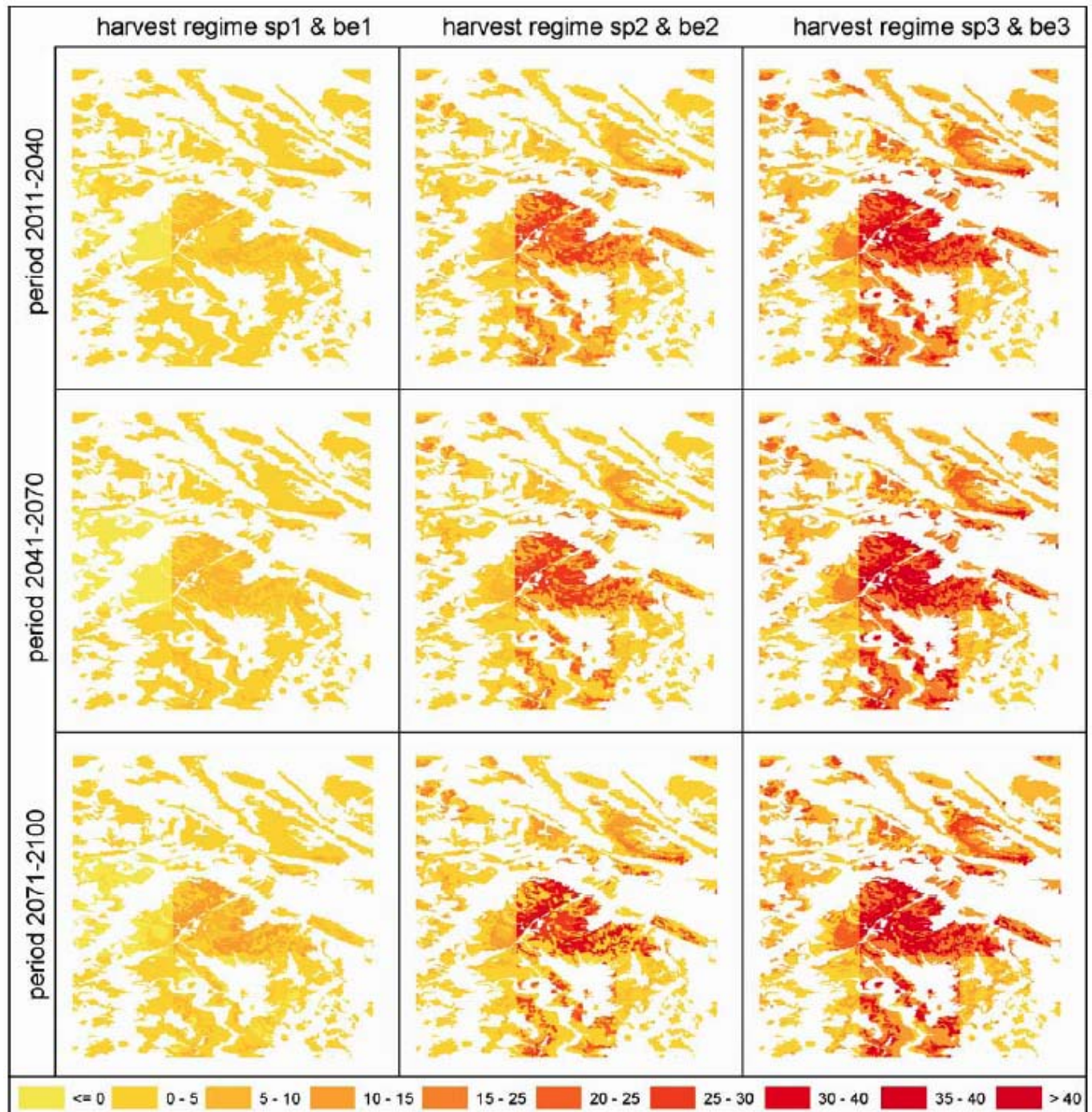


Fig. (6). Spatial and temporal variations of wind damage risks (%) in forest ecosystems for different target diameter harvest regimes under A1B climate change conditions, presented as differences between mean annual wind risks for a given period and P0.

CONCLUSIONS

The present study has shown that according to the climate scenarios A1B and B1 regionalized with CLM the air temperature in Solling area is likely to increase monotonically towards 2100. The changes are considerable – up to 37% under A1B and up to 25% under B1. The changes of precipitation are within 6.5 % only whereas the maximal increase is projected for P1 (2011-2040). The wind speed is likely to increase weakly – up to 1.6% compared to present conditions. Therefore, in unmanaged stands the increment of

wind risks towards 2100 compared to “present climate conditions”, is mainly caused by the changes in annual precipitation and increase of mean air temperature. However the temporal course of risks development depends on the evolution of windspeed.

Among the non-meteorological variables determining risks of windthrow the key factors are the distance between trees, h/DBH ratio, rooting depth and soil moisture.

The risks for unmanaged spruce are higher than for beech stands and the risks for beech stands start to decrease after

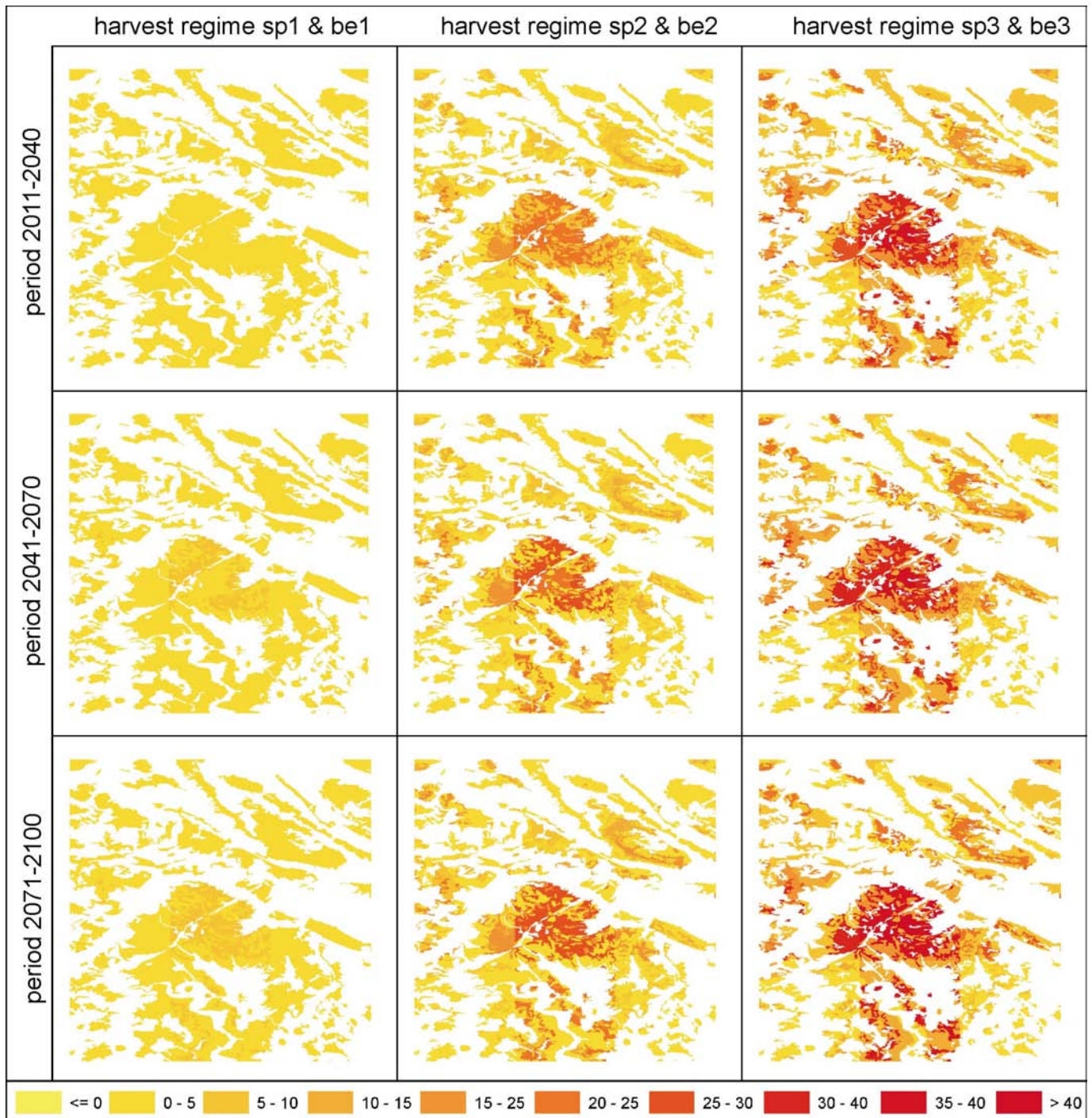


Fig. (7). Spatial and temporal variations of wind damage risks (%) in forest ecosystems for different target diameter harvest regimes under B1 climate change conditions, presented as differences between mean annual wind risks for a given period and P0.

2040. Thus it could be concluded that for different locations and combinations of meteorological variables different key factors will control the magnitude and the distribution of wind risks. The spatial distribution of damage and its dynamics depend on the superposition of forest types, soils and climatic variables. Therefore the estimation of wind damage risks should be carried out using a coupled model taking into account the dynamic of soil moisture, structural properties for considered tree species and their temporal variability and the dynamic of climatic parameters. It was

shown that the proposed method of DSS-WuK demonstrates the ability to describe all mentioned processes. When implemented to the evaluation of wind risks in the managed stands the DSS has shown that the forest management method – TDH tends to destabilize forest stands remaining after harvesting and thus – to increase the future wind damage risks. The higher is the intensity of harvesting – the more unstable against wind stress will be the remaining stand.

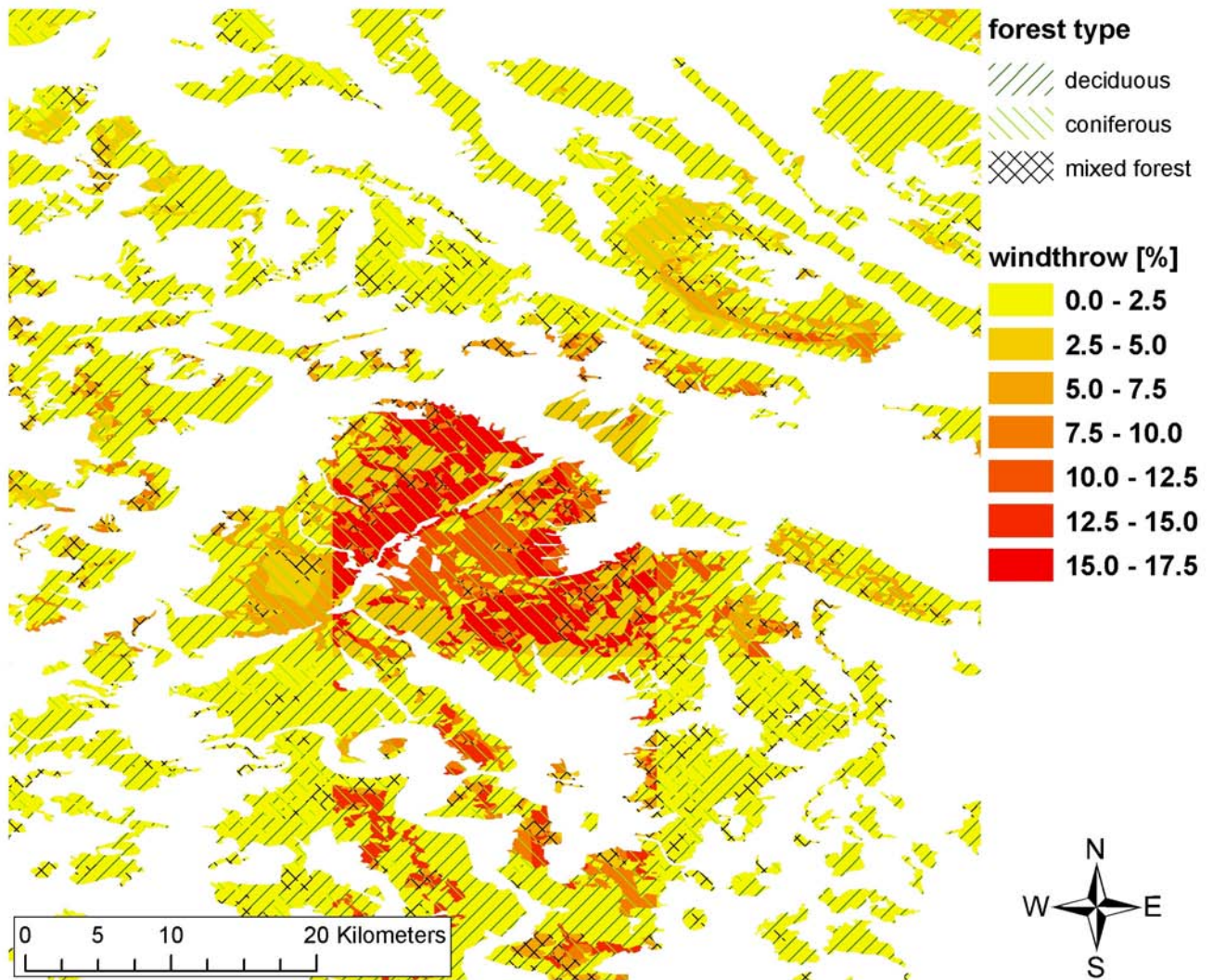


Fig. (8). Superposition of spatial distributions of forest types and wind damage risks in forest ecosystems for reference scenario P0.

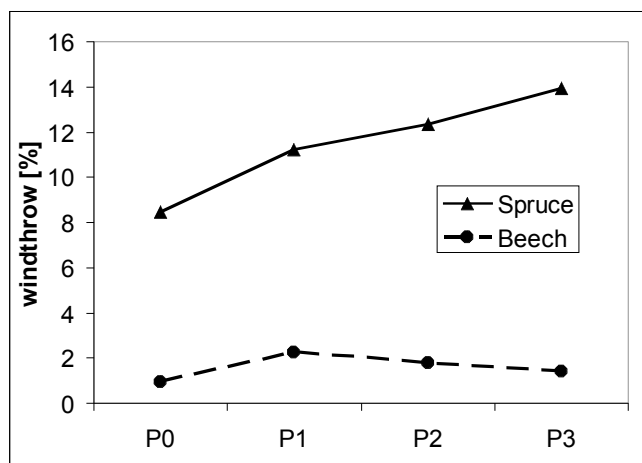


Fig. (9). The changes of scenario-averaged 30-years mean values of windthrow damage in Solling area for Norway spruce and European beech.

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