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**RESEARCH ARTICLE**

The Effect of CaBr_2 on Mercury Speciation in Flue Gas: An Experimental and DFT Study

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Abstract:**Background:**

Additives affect the formation of different mercury speciation in coal-fired derived flue gas.

Objective:In order to study the effect of the additive CaBr_2 content, the Ontario Hydro Method (OHM) method has been applied to analyze the mercury speciation at the entrance and export of denitration (SCR).**Method:**

Density Functional Theory (DFT) has been used to study the adsorption of mercury halide on unburned carbon surface.

Result:The results show that along with the increasing amount of additive CaBr_2 , there is an increasing trend of the ratio of Hg^{2+} in flue gas.**Conclusion:** CaBr_2 addition contributes to oxidize Hg^0 to Hg^{2+} and increase the mercury concentration through SCR. DFT results indicate that the adsorption of HgBr and HgBr_2 on unburned carbon surface is chemisorption, and Br-C bond is stronger than Hg-C bond, both these bonds are covalent interaction.**Keywords:** Additive CaBr_2 , Mercury speciation, Flue gas, DFT, AIM, Ontario Hydro Method (OHM).

1. INTRODUCTION

The poisonous and heavy metal of mercury is a global pollutant, which endangers ecological environment and the health of human [1]. Coal combustion is the major anthropogenic source of the mercury emission, and the estimated 3400 tons of mercury emitted from coal-fired power plants in 2010 year [2 - 4]. The deep research of reaction and migration mechanisms of mercury in coal-fired power plants flue gas and fly ash is of great significance to effectively control mercury emission.

There is a certain amount of mercury in coal, which emissions into flue gas in burning. Along with the combustion of coal, almost mercury emitted in the form of gaseous elemental (Hg). In the furnace flue tail, the elemental mercury (Hg^0) is oxidized to divalent mercury (Hg^{+2}) with the decreasing of flue gas temperature. Elemental and divalent mercury may adsorb on unburned carbon and then convert into particulate mercury (Hg_p) [5 - 8]. In the progress of coal

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combustion, the enrichment and distribution form of mercury species were affected by many factors, such as types and composition of coal, characteristics of fly ash, composition of flue gas, operation conditions of boiler and burning temperature. In detail, the content of gas Hg^{2+} is higher than Hg_p in bituminous coal flue gas, but in sub-bituminous coal flue gas, the content of gas Hg^0 and Hg_p are both high, which the reasons may be the component of flue gas and fly ash in the bituminous coal has strong oxidation to Hg^0 , and the constituents of flue gas and fly ash in sub-bituminous coal has strong adsorption to Hg^0 . Mercury species present enrichment state on the fly ash surface, the smaller particle size of fly ash, the larger specific surface area of ash particle, and the more mercury adsorbed on ash particle. In addition, the pore structure of ash particle affects the adsorption capacity of mercury, in which the large porosity is advantageous to mercury adsorption. Active inorganic chemical component in fly ash plays an important facilitating role in mercury oxidation and capture. Ghorishi [9] revealed that the Fe_2O_3 has strong oxidation to Hg^0 , but the Al_2O_3 , SiO_2 and CaO have relatively few oxidation to Hg^0 . Moreover, transition metal oxides of CuO and MnO_2 also have promoting effect on mercury oxidation [10, 11]. Gaseous SO_x as a major component of flue gas, it also affects mercury oxidation. Preso [12] proposed that SO_3 has strong inhibitory effect on mercury capture in the condition of low concentration of SO_3 , which the reason is the competitive adsorption between SO_3 and Hg^0 on active sites. Diamantopoulou [13] considered that SO_2 can promote the mercury capture by fly ash due to the SO_2 which increases sulfur contained active sites on active carbon. Many studies have been conducted on the effect of halogen promoting mercury oxidation, confirming that chlorine, presented as HCl , Cl_2 or Cl radicals in the flue gas, contributes to Hg^0 oxidation [14]. Agarwal [15] investigated the influence of H_2O , SO_2 and NO on Hg^0 oxidation when the Cl_2 as oxidant, the results showed that the H_2O , SO_2 and NO make inhibition effect on Hg^0 oxidation. The HCl content is considered a vital factor that affects the mercury oxidation. Ochiai [16] studied the influence of HCl on mercury adsorption on active carbon surface based temperature programmed desorption experiment, the experimental results indicated that HCl presents promoting effect on mercury adsorption, and HCl concentration plays an important role in mercury species distribution, which may be the reasons for the formation of HgCl_2 by direct reaction between HCl and Hg^0 or indirect reaction between HCl and HgO . Moreover, Galbreath [5] investigated the influence of HCl on mercury species transformation by injecting HCl into various flue gas which produced by burning bituminous coal, sub-bituminous coal and lignite, the experimental results showed that the injected HCl prominently promotes oxidation of Hg^0 to Hg^{2+} in sub-bituminous coal flue gas, but the injected HCl promotes oxidation of Hg^0 and Hg^{2+} to Hg_p in lignite flue gas. The same effect is also detected with bromine since Cl and Br are congeners sharing similar properties [17]. Br can promote mercury oxidation and have the highest oxidation capability than Cl and other halogen [18 - 19]. In detail, Cao [18] researched the oxidation ability of HF , HCl , HBr and HI to Hg based the sub-bituminous coal flue gas, the results showed that oxidation ability are $\text{HBr} > \text{HI} \gg \text{HCl} \sim \text{HF}$, a little added HBr in flue gas can make a contribution to 90% mercury oxidation rate. Liu [19] studied the synergism effect of Br_2 and fly ash on mercury oxidation, the results showed that Br_2 can facilitate the mercury oxidation, but Br_2 mixed with fly ash especially for unburned carbon that can remarkably promote the mercury oxidation. The added bromine promotes mercury adsorption on fly ash and unburned carbon particle, and then facilitates heterogeneous oxidation reaction. In addition, the bromine salt is easier to decompose for participation in mercury oxidation. Comparing with the study of the effect of chlorine, there are still scarce conducted on Br , especially in field experiments. Also, SCR catalyst is another important factor in this process, promoting mercury oxidation as well as providing adsorption sites. Unburned carbon can provide active sites for the adsorption of bromine and mercury [20, 21], which promotes the oxidation of elemental mercury.

In the flue gas, mercury presents three forms which are element mercury, divalent mercury and particulate mercury. Particulate mercury (Hg_p) does not have water-solubility and it can be removed by dust control equipment. Divalent mercury (Hg^{2+}) is soluble in water and it can be removed by wet flue gas desulfurization devices. Elemental mercury

Hg⁰ is not soluble in water and difficult to be removed [8, 22, 23]. Therefore, promoting the Hg⁰ convert into Hg²⁺ and Hg_p is beneficial ecologically and has been the research focus of domestic and abroad scholars.

To sum up, the previous studies mostly focused on the effect of HCl or HBr on mercury oxidation and were carried out in simulated flue gas, there have been not enough researches on the contribution of CaBr₂, as well as the oxidizing action on mercury of additives with different concentrations. Stated thus, in order to study the influence of additive CaBr₂ on mercury speciation in flue gas, the additives experiment was carried out based on one 300 MW coal-fired boiler, the Ontario Hydro Method (OHM) was utilized to sample mercury at the denitration entrance and export., and the variation of mercury before and during adding the additives was captured and the effect of the additives was analyzed. In addition, Density Functional Theory (DFT) computational study was used to theoretically analysis mercury oxidized by bromine on unburned carbon surface.

2. EXPERIMENTAL AND COMPUTATIONAL DETAILS

2.1. Experimental Condition

The CaBr₂ addition experiments were conducted in one 300MW boiler of #1 unit in the power plant, whose annual power generation is 6~8 billion kW·h. This 4×300MW unit plant adopts first medium reheating natural circulation drum boiler under subcritical pressure, equipped with the pollution control facilities and installations, such as the electrostatic precipitator, SCR denitrification and desulfurization devices, etc.

Sampling points were set at SCR entrance and export as shown in Fig. (1). CaBr₂ was fed with a screw feeder to vibration coal feeder. The flue gas was extracted from sampling points for thirty minutes for mercury collecting. At SCR entrance and export sampling points, the Ontario Hydro Method (OHM) [24] was applied. The ash particles were permeated *via* a heated quartz filter membrane, and then passed through three adsorbing bottles in turn, which one is 1 mol/L KCl solution, one with 10% H₂O₂-5% HNO₃ solution and another one is 4% KMnO₄-10% H₂SO₄ solution. These solutions were used to adsorption for Hg²⁺ and Hg⁰. And the absorption liquid was taken back to the laboratory immediately for digestion and finally was collected in Teflon bottles. The RA-915 type mercury analyzer of LUMEX company was used for measuring mercury content in all the samples.

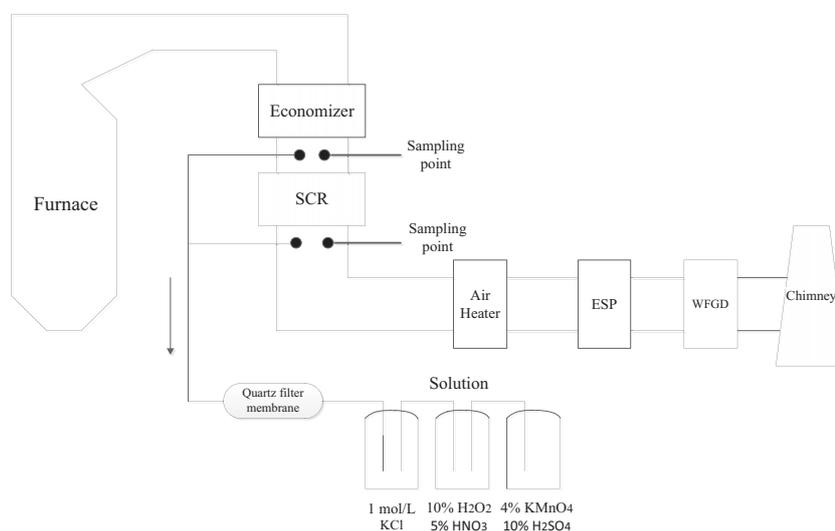


Fig. (1). CaBr₂ addition experiments schematic.

Serial numbers C1 to C6 represent condition one to condition six, respectively. In detail, there is no CaBr₂ addition in C1. From C2 to C6, the amount of CaBr₂ increases gradually and the specific dosage is shown in Table 1. Proximate analysis and mercury content of coal sample are shown in Table 2.

Table 1. CaBr₂ addition amount.

Conditions	C1	C2	C3	C4	C5	C6
CaBr ₂ addition amount(kg/h)	0	0.5	1.5	5	15	50

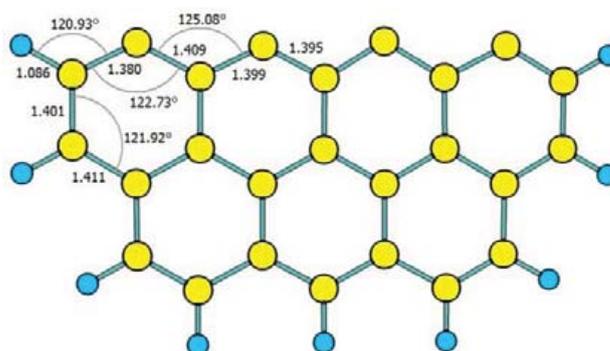
Table 2. Proximate analysis and mercury content of coal.

Moisture	Ash(A _{ar})	Volatility(V _{ar})	Fixed carbon(FC _{ar})	Mercury(ng/g)
15.56	10.52	28.92	41.16	46.8

2.2. Computational Details

Single layer graphene model was used to simulate unburned carbon surface, which has been proven that it provides satisfactory results for relevant reaction mechanisms of carbon based surface [25, 26]. As shown in Fig. (2), seven-ring benzene cluster model of Zigzag was applied to simulate unburned carbon in flue gas in this paper, and the active sites of this model were not saturated by hydrogen. Density functional theory B3LYP method [27] was used to the optimization of configuration and calculation of energy. In detail, pseudopotential basis set SDD was used to mercury atom, and the Pople 6-31G(d) basis set was applied for non-metal elements (C, H and Br) [25]. In this paper, all of the calculation was carried out by Gaussian 09 program [28]. The adsorption energy was calculated by equation (1):

$$E_{ads} = E_{model+adsorbate} - E_{model} - E_{adsorbate} \quad (1)$$

**Fig. (2).** Seven-ring benzene cluster model.

Yellow and blue ball represent carbon and hydrogen atom, respectively.

Where $E_{model+adsorbate}$ is the total energy of adsorption complex of benzene cluster model and adsorbate, E_{model} and $E_{adsorbate}$ are the energy of benzene cluster model and adsorbate, respectively. Negative value of E_{ads} represents the adsorption progress is exothermic, and higher negative values of E_{ads} reflects the stronger adsorption capacity of benzene cluster model onto adsorbate [29, 30].

In addition, Atoms in Molecules (AIM) method [31, 32] was used to analyze the type and strength of bond between unburned carbon model and adsorbates. AIM was evaluated by wave function analysis program of Multiwfn 3.2.1 [33], and isosurface maps of adsorption complexes were plotted by VMD program in this paper [34].

3. RESULTS AND DISCUSSION

3.1. Effect of CaBr₂ Addition on Mercury Speciation at SCR

The concentrations of gaseous mercury at the SCR entrance and export in different experimental conditions are shown in Table 3. It is clearly observed that before entering SCR, mercury is mainly presented as Hg⁰ in the flue gas, which has been confirmed by S. Niksa [35].

Table 3. Gaseous mercury concentration at SCR in different conditions.

Condition	Addition Amount (kg/h)	Measuring Position	Hg (g) Concentration (ug/m ³)	Hg ²⁺ (g) Concentration (ug/m ³)
C1	0	Entrance	8.26	0.83
		Export	1.38	3.21
C2	0.5	Entrance	2.42	0.32
		Export	2.71	1.69
C3	1.5	Entrance	1.22	0.34
		Export	2.04	2.64
C4	5	Entrance	0.91	0.43
		Export	0.95	4.54
C5	15	Entrance	0.83	0.46
		Export	0.38	5.24
C6	50	Entrance	1.04	0.44
		Export	0.59	2.59

In Table 2 it can be found that the mercury mass fraction is 46.8 ng/g, and mercury exists in three forms: elemental mercury, divalent mercury and particle mercury. During the combustion of coal, variant mercury species decompose and release gaseous mercury into flue gas. Lopez-Anton [36, 37] demonstrated that HgCl₂, HgS, HgO and HgSO₄ are the main mercury species in coal-fired ash and gas. In detail, the thermal decomposition temperature of HgCl₂ is 70°C. There are two different forms of crystal structure, black cube HgS and red six party HgS, which decompose at the temperature of 170°C and 240°C, respectively, the component HgO and HgSO₄ decompose at the temperature of 200°C and 500°C. In addition, mercury species of Hg₂SO₄ and Hg₂Cl₂ also exist in ash and flue gas, but Hg₂SO₄ and Hg₂Cl₂ are unstable.

In condition one in Table 3, in which the gaseous Hg⁰ and Hg²⁺ concentrations are 8.26 μg/m³ and 0.83 μg/m³, respectively, it means mercury mainly exists in Hg⁰ form. In detail, the mercury component Hg₂SO₄ easily decomposes to Hg and HgSO₄, Hg₂Cl₂ easily decomposes to Hg and HgCl₂, as shown in equations (2) and (3):



Similarly, the HgCl₂, HgS, HgO and HgSO₄ in fly ash and flue gas decompose into element mercury and other substance at high temperature. Along with the temperature of flue gas decreases, the decomposition of almost mercury species is halted, and mercury oxidation dominates gradually. Due to the halogen and sulfur consist in flue gas, the homogeneous oxidation reaction of element mercury to oxidized mercury are occurred, such as shown in equations (4) to (7) [38].



Where the (g) represents gaseous phase. Hg⁰ can be oxidized to HgCl by gaseous HCl and Cl₂, and then some HgCl be oxidized completely to HgCl₂. In addition, heterogeneous oxidation reactions between chlorine and element mercury on ash particle are shown in equations (8) to (11) [39].





Where the (ad) represents substance adsorbed on ash or unburned carbon particle.

In addition, Hg^0 also can be oxidized by sulfur. Rubel demonstrated that a good correlation exists between sulfur and mercury capture. He proposed that the unburned carbon released from high sulfur coals have shown to have higher mercury adsorption capacity than that from low sulfur coals. H_2S and SO_2 play an important role in oxidizing mercury in flue gas, the detailed oxidation reaction as shown in equations (12) to (14) [40].



H_2S can be oxidized to S^0 by oxygen or SO_2 on ash or unburned carbon surface, and then adsorbed sulfur can capture Hg^0 , and finally, HgS may adsorb on ash surface to form particle mercury or releases into flue gas to form gaseous oxidized mercury. To sum up, the massive element mercury and a little oxidized mercury released during the coal combustion, so the Hg^0 concentration is larger than Hg^{2+} concentration at the SCR entrance. Along with the temperature of flue gas decreased, the oxidation of mercury is dominant than decomposition, so the Hg^{2+} concentration is larger than Hg^0 concentration at the SCR export.

In each condition, there is an increase of Hg^{2+} and conversely, a decrease of Hg^0 in flue gas at SCR export compared with entrance, which means the oxidation of Hg^0 to Hg^{2+} taken place in the SCR. Almost all of the mercury leaving furnace is presented in element form in flue gas with high temperature, whose oxidation from the elemental form to divalent form takes place as the temperature decreases and gets promoted under the effect of halogen in the coal and SCR catalyst. Divalent mercury is more strongly adsorbed on the surface of both ash particles and SCR catalyst than element mercury [41]. As clearly shown in C1 in Table (3), the increase of gaseous divalent mercury amount in the flue gas is less than that of decrease of gaseous element mercury and the total gaseous mercury concentration through SCR, which the reasons may be that the gaseous Hg^{2+} adsorbed on unburned carbon and SCR catalyst surface. With the additive CaBr_2 has been added in C2, the Hg^0 and Hg^{2+} concentration decreased in SCR entrance which compared with C1. The Hg^0 concentration decreased which dues to the oxidation of Hg^0 to Hg^{2+} by CaBr_2 , but the Hg^{2+} concentration did not increase but decrease, which the reasons may be that the CaBr_2 promotes the adsorption of Hg^{2+} on unburned carbon surface. In addition, the Hg^{2+} concentration in SCR export is higher than that in SCR entrance in C2, which means that the SCR catalyst can promote the oxidation of Hg^0 to Hg^{2+} . From C2 to C5, as CaBr_2 addition amount increases, the proportion of Hg^{2+} increases as well both at SCR entrance and export, at the same time, the Hg^0 proportion decreases at SCR entrance, experimental results indicate that CaBr_2 can facilitate the oxidation of Hg^0 to Hg^{2+} in general. Especially, C5 reached the extreme point among these conditions and although more CaBr_2 was added in C6, the proportion of Hg^{2+} in C5 is larger than that of C6 both at SCR entrance and export, the reason of which is mainly that the CaBr_2 addition amount has reached a saturation value beyond and thus the oxidation is no longer enhanced [4, 42].

Fig. (3) shows the variation of Hg and Hg^{2+} concentration decrease rate at SCR entrance alone with the increase of CaBr_2 addition amount. As shown in Fig. (3), with the additive CaBr_2 has been added, the gaseous Hg concentration decreased. In C2, CaBr_2 with addition level of 0.5 kg/h was added in flue gas, the reduction rate of gaseous Hg^0 concentration at SCR entrance is 70.7% comparing with that of C1. Similarly, the reduction rates of gaseous Hg^0 of C3, C4, C5 and C6 are 85.2%, 89.0%, 90.6% and 87.0%, respectively. Analyzing these reduction rates of different conditions, it can be found that the gaseous mercury concentration decrease rapidly along with the increase of CaBr_2 addition level in general, which indicates that additive CaBr_2 can oxidize Hg^0 to Hg^{2+} , these findings agree with previous studies [43, 44]. Interestingly, along with the increase of CaBr_2 addition amount, the gaseous Hg^{2+} concentration is not increase but decrease at the SCR entrance, the reasons may be that the additive CaBr_2 contributes to more fly ash in flue gas, and more oxidized Hg^{2+} adsorb on ash particles, which makes the decrease of Hg^{2+} concentration at SCR entrance.

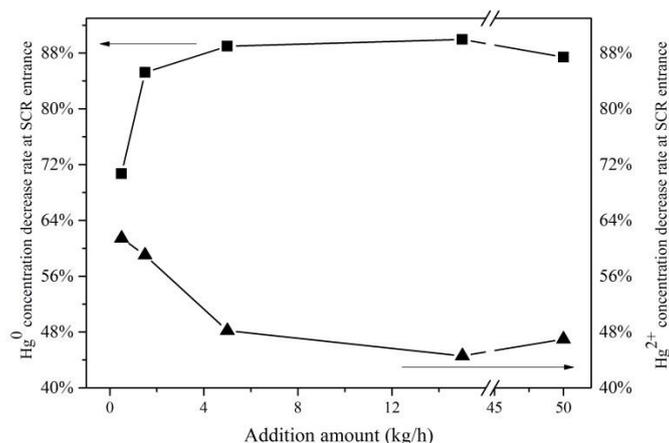


Fig. (3). Variation of Hg⁰ and Hg²⁺ concentration decrease rate at SCR entrance versus CaBr₂ addition amount.

Fig. (4) shows the variation of Hg²⁺ concentration increase rate at SCR export along with the increase of CaBr₂ addition amount. As shown in Fig. (4), whether or not to add additive CaBr₂, the gaseous Hg²⁺ concentration all increased. In C1 which there is no CaBr₂ addition, the increase ratio of Hg²⁺ concentration between SCR export and entrance has reached to 74%, probably because that in C1, with quite little halogen in coal and the subsequent in flue gas, almost all the mercury oxidation is conducted in SCR while halogen contributes to mercury oxidation. Along with the increase of CaBr₂ addition amount, the increase rate of Hg²⁺ concentration also increases, and in C5 which the CaBr₂ addition amount is 15 kg/h, the increase rate reaches the maximum value, which indicates that the oxidation reaction is saturated. In C6, with the CaBr₂ addition amount continues to increase to 50 kg/h, the Hg²⁺ concentration increase rate has decreased to 82.4%.

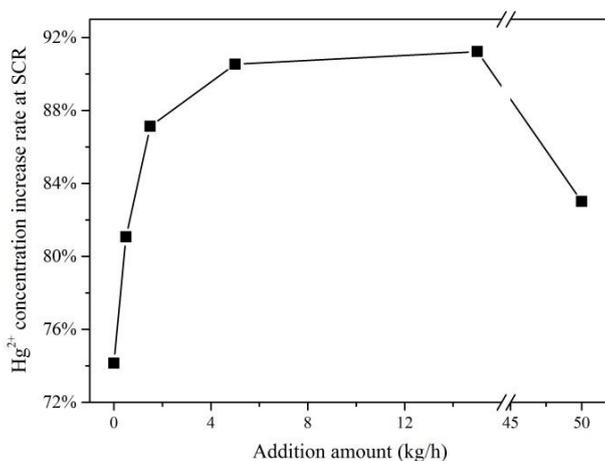


Fig. (4). Variation of Hg²⁺ concentration increase rate at SCR versus CaBr₂ addition amount.

The subsequent products such as CaO and Ca(OH)₂ may be produced because of CaBr₂ addition as shown in equation (15) to (16), and these subsequent products are effective of Hg²⁺ adsorbents. Flue gas leaving the furnace with high temperature, bromine is presented mainly as HBr [41], and as the gas temperature decreases, Br atoms are in a concentration [4] and in the subsequent cooling process Br₂ is formed. Therefore in the flue gas leaving the furnace before entering SCR, HBr is the most speciation of bromine. In addition, the HBr released from the reaction of CaBr₂ and H₂O, the reaction as shown in equations (15) and (16).



Both homogeneous and heterogeneous chemistry exist in Hg⁰(g) oxidation. In the flue gas, according to what

Stephen [4] has found, Hg^0 is first partially oxidized by Br atom into HgBr and then oxidized into HgBr_2 by Br_2 . Since the concentration of Br_2 is smaller than that of Br atoms in high temperature flue gas, homogeneous oxidation results in most mercury being presented as HgBr(g) with a small amount of HgBr_2 . Gao [23] proposed that in the flue gas leaving the furnace before entering SCR, most bromine is presented in HBr and a small part in Br atoms with tiny amount of Br_2 . Stephen [4] presented that Hg homogeneous chemistry with Br species is much faster than with Cl species because the Br atom concentrations at the furnace exit are three to four orders of magnitude greater, the dominant channels with Br are analogous to those for Cl, whereby a Br atom partially oxidizes Hg^0 into HgBr. In addition, mercury also oxidizes heterogeneously on unburned carbon with Br species. Raik [41] suggested that in the subsequent cooling process, the fuel bromine or added bromine is eventually transformed into HBr. Based on the DFT calculation, Padak's [47] results for Hg adsorption in the presence of chlorine, it was found that HgBr species are more stable on the unburned carbon surface than HgBr_2 species. Fujiwara [35] proposed that heterogeneous Hg^0 oxidation on unburned carbon is usually the essential inherent mechanism to oxidize Hg^0 in coal-derived flue gas. Bench-scale experiments [45] and quantum chemistry theoretical studies [46] have indicated that heterogeneous mercury oxidation is at least 90% proportion of the overall oxidation in coal-fired flue gas. Heterogeneous reaction is mainly determined by adsorption on Unburned Carbon (UBC) surfaces, and the oxidation mechanism is as follows:



Where (g) and (ads) represents gaseous and adsorption state, respectively [4].

Since most bromine is in HBr form in the high temperature gas, which is easily adsorbed on unburned carbon surface *via* equation (17). And then, gaseous element mercury is adsorbed on carbon surface through the interaction with Br(ads). In addition, HgBr(ads) may be oxidized further into $\text{HgBr}_2(\text{ads})$ by gaseous HBr. Padak [47] confirmed that HgBr is more strongly and stably adsorbed on the unburned carbon surface than HgBr_2 by quantum chemistry calculation. Gale *et al.* [48] found that the Ca enhances mercury capture by preventing Hg^{2+} desorption from carbon surface. Therefore, due to homogeneous and heterogeneous chemistry, in the high temperature gas before entering SCR, mercury presented mainly in HgBr form, most of which is adsorbed on UBC surface.

According to the Deacon reaction: $4\text{HCl} + \text{O}_2 \rightarrow 2\text{H}_2\text{O} + 2\text{Cl}_2$, when the flue gas enters SCR, Cl_2 is produced under the effect of the vanadium-based catalyst. There has been no specified reaction in bromine situation and it is predicted here that the concentration of Br_2 begins to increase in SCR as flue gas temperature decreases [4]. Both the homogeneous and heterogeneous mercury oxidations exist in SCR. According to Hein [41], homogeneous mercury oxidation in SCR involves $\text{Hg}^0(\text{g})$ reacting with HBr to produce $\text{HgBr}_2(\text{g})$. Since mercury in the flue gas entering SCR is mainly in HgBr(ads) form, no big $\text{Hg}^0(\text{g})$ concentration variation is supposed to be detected. Mercury oxidation in SCR is mainly in heterogeneous chemistry [39].

The produced Br_2 in SCR is a strong oxidant and can easily oxidize adsorbed HgBr into HgBr_2 which then gets desorbed. Also the remained HBr may react with HgBr(ads) to form $\text{HgBr}_2(\text{g})$ *via* equation (20) [4] and therefore $\text{Hg}^{2+}(\text{g})$ concentration in SCR increases.



On the other hand, two reaction mechanisms have been previously proposed for mercury heterogeneous oxidation on vanadium-based SCR catalyst surface. Senior [49] applied Eley-Rideal mechanism which indicates that adsorbed mercury on catalyst surface reacts with hydrogen halide in the flue gas, while Hein *et al.* [41] have mentioned Langmuir-Hinshelwood mechanism that Hg^0 and hydrogen halide both are adsorbed on catalyst surface firstly, and then start to react. When hydrogen halide concentration is much larger than element mercury, mercury oxidation on the SCR catalyst surface is mainly dominated by Langmuir-Hinshelwood mechanism because of the higher affinity of hydrogen halide with the active sites in SCR catalyst than mercury [50]. Therefore compared to HBr in the flue gas, there are not much Hg^0 and Hg^{2+} adsorbed on SCR catalyst surface. Abad-Valle *et al.* [51] found that hydrogen halide binds itself to carbon particle surface prior to Hg, indicating that not much $\text{Hg}^{2+}(\text{g})$ is adsorbed on unburned carbon surface. Through analyzing heterogeneous and homogeneous mercury oxidation and adsorption on the unburned carbon and SCR catalyst

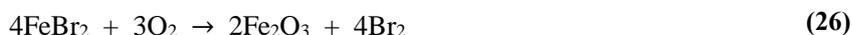
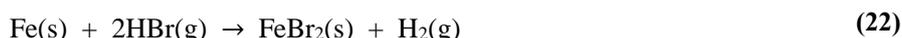
surface, it is shown that CaBr₂ addition contributes to an increase of element mercury transform into divalent mercury.

The dominant forms of Hg in coal-fired flue gas are Hg⁰ and Hg²⁺ [52], and the fraction of Hg²⁺ in flue gas depends on the coal quality, boiler loads and so on. Hg⁰ can be oxidized to HgCl and HgCl₂ by Cl₂ and HCl, respectively. HCl is the major Cl species under the condition of SCR operation [4]. HCl is more stably adsorbed on SCR catalyst surface than Hg, which means that the HCl inhibits the mercury adsorption on catalyst surface [53]. Generally, element mercury on SCR catalyst oxidizes faster than that on unburned carbon under the condition of chlorine level is moderate or higher.

Since the unburned carbon can enhance mercury capture, different coal ranks with dissimilar unburned carbon content in flue gas have different results in mercury capture. The combustion results of anthracites coal and bituminous coal show that the unburned carbon in fly ash is anisotropic, unresolved and dense. On the contrary, the structure of unburned carbon in fly ash is isotropic and porous, which formed from subbituminous or lignite. The different characteristics of unburned carbon greatly affect the mercury capture, the UBC with anisotropic fused structure is more favorable for adsorbing mercury. Gale [48] found that much more mercury oxidation can be realized by blending coal, even though there was less chlorine. The reasons may be that the added bituminous coal yields more unburned carbon in the ash, which enhances mercury oxidation. In addition, low-rank coal with high concentration of calcium can promote mercury oxidation. Gale [48] proposed that calcium can enhance the HgCl adsorption on the unburned carbon surface and element mercury adsorption onto chlorinated-carbon sites.

Temperature affects mercury capture *via* the unburned carbon formation in the boiler with high temperature to the quenching environment of flue gas. In addition, homogeneous Hg oxidation by Br begins as the flue gas cools below 600°C [4]. Subtle changes in boiler operation condition can potentially results in significant changes for unburned carbon properties [54], and these changes may impact mercury capture in fly ash.

It is well known that chlorine can cause serious corrosion to boilers, heater exchangers and pipes surface as a result of complex chemical interactions between species like HCl, Cl₂, H₂O, O₂ and metal [55, 56]. Similar to chlorine-associated corrosion, bromine may cause corrosion depending on the flue gas conditions. Element bromine is injected *via* the addition of CaBr₂, and HBr is the primary Br species in the gas phase and little Br₂ may be present at higher temperature. Both the HBr and Br₂ can react with metal to form metal bromides. The oxidation mechanisms can be revealed *via* the equation (21) to (26) [57].



Stated thus, the CaBr₂ addition has caused corrosion to the metal of boiler, which makes the negative effect on the stable operation of heat exchange pipes. The present of HBr and Br₂ can thin the pipe walls and reduce the structural strength of metal pipes. Although the additive CaBr₂ can promote the mercury oxidation, the corrosion characteristic of HBr which formed from CaBr₂ also should be considered.

3.2. DFT Calculations

In order to gain further insight into the adsorption mechanisms of mercury and halogen on the unburned carbon surface, the reaction path of Hg on Zigzag carbon model which adsorbed single bromine atom has been studied, in addition, the adsorption complex of Zigzag···HgBr₂ has been optimized.

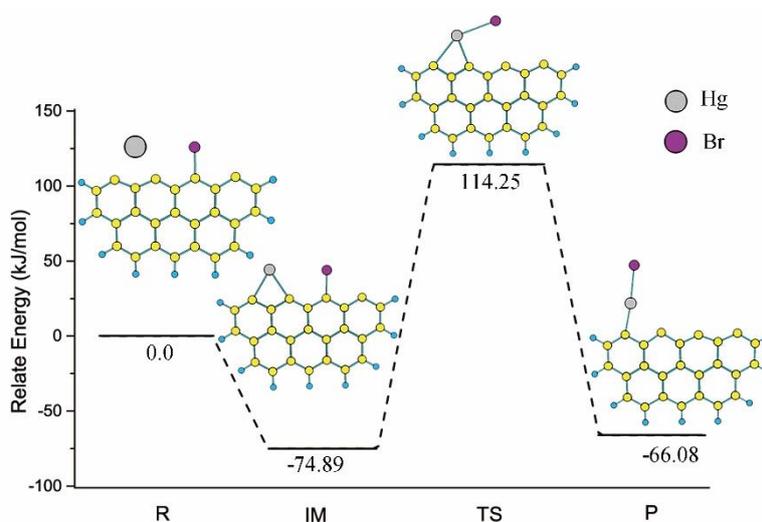


Fig. (5). The reaction path of Hg and $C_{25}H_9$ -Br model.

R, IM, TS and P represents reaction, intermediate, transition state and product.

According to the Equation (18), the generation path of adsorbed HgBr *via* gas Hg and Zigzag-Br model has been shown in Fig. (5). Gas element mercury chemically adsorbed on active sites which on the side of Br atom, and corresponding adsorption energy is 74.89 kJ/mol. In transition state structure of TS, the bond between active site and Br atom broken, and the Br atom closed to the adsorbed Hg atom. The structure of TS is not stable and corresponding energy is higher 114.25 kJ/mol than that of reactants. TS quickly converts into final product along with the Br atom far away from active sites. The total energy of final product is lower 66.08 kJ/mol than that of the reactants. The theoretic DFT results have verified the validity of Equation (18) and indicated that the adsorption of gas Hg^0 on carbon model which adsorbed Br is chemisorption.

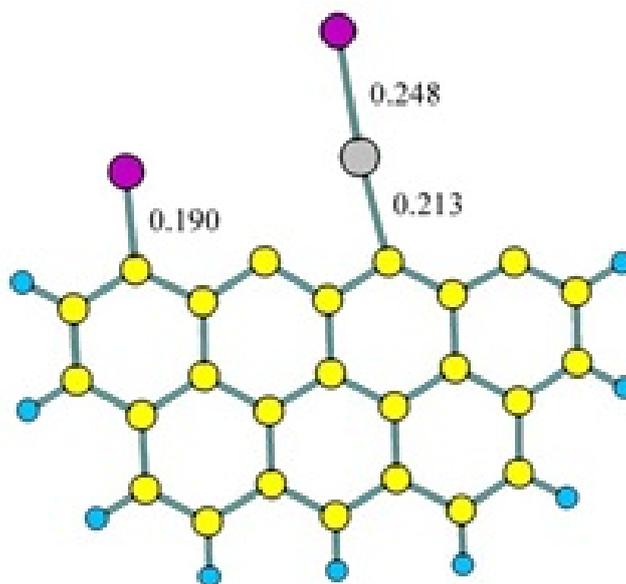


Fig. (6). The adsorption configuration of $HgBr_2$ on $C_{25}H_9$ model.

The optimization complex of $HgBr_2$ adsorbed on Zigzag carbon model surface is shown in Fig. (6). One of the Hg-Br bond broken, Br atom and Hg atom adsorbed on active sites, respectively. The adsorption energy of $HgBr_2$ on Zigzag carbon model surface is 325.46 kJ/mol, indicates that the adsorption is chemisorption. As shown in Fig. (4), the bond length of Br-C and Hg-C is 0.190 nm and 0.213 nm, respectively, the bond strength of Br-C may stronger than that of Hg-C. This adsorption configuration may be formed *via* the oxidation reaction of Br atom and Zigzag -HgBr complex.

Atoms in Molecules (AIM) theory has been successfully and widely used to study the properties of shared-shell (covalent) and closed-shell bonding [58, 59]. This theory depicts that the Hessian matrix of the charge density can be well applied to evaluate characterize of a bond. The bond critical point (BCP) is the laplacian of the charge density, which is the sum of three eigenvalues of Hessian matrix. According to the criteria proposed by Carroll and Bader [60, 61] based on charge density topology, there are some regulations can be used to analysis the bond characterize. First, the presence of BCP between two atoms indicates that the existence of bond path between these two atoms. Second, the value of charge density at BCP is positively correlated with the binding energy for hydrogen bond and covalent bond. Third, the positive and negative values of laplacian of the charge density at the BCP are indicative of closed-shell and covalent interaction, respectively. In addition, Cremer suggested that potential energy density $V(r)$, Lagrangian kinetic energy $G(r)$ and total energy density $H(r)$ ($H = V + G$) can be used to distinguish the covalent and closed-shell interaction. In detail, $|V(r)| > G(r)$ and $H(r) < 0$ is indicative of covalent interaction, conversely, $|V(r)| < G(r)$ and $H(r) > 0$ is indicative of closed-shell bonding.

The BCPs between HgBr and carbon model have been shown in Fig. (7a), which indicates that the bond paths existed between these interaction atoms. The results of charge density topological analysis have been shown in Table 4. In the configuration of HgBr adsorbed on carbon model surface, the sign of $\nabla^2\rho(r)$ at both BCPs of Hg-C bond is positive, which indicates that the bonding between Hg atom and active site is covalent interaction. In similarly, the positive sign of $\nabla^2\rho(r)$ of Hg-Br bond in this configuration is indicative of covalent bond. According to the Cremer's criterion, the BCP of Hg-C and Hg-Br bonds with characteristic of $|V(r)| > G(r)$ and $H(r) < 0$ as shown in Table 4, which demonstrated that these bonding are covalent interaction. The value of charge density ρ at the BCP of Hg-C_2 bond is larger than that of Hg-Br bond, demonstrating that the bonding strength of Hg-C bond is stronger than that of Hg-Br bond. The same analysis has been conducted to the configuration of HgBr_2 adsorbed on carbon model as shown in Fig. (7b), it can be concluded that the bonding of Br and C atom belongs to covalent interaction, and the Br-C bond is stronger than Hg-C and Hg-Br bonds. Analyzing the values of G , V and H , it can be also found that these bonds are covalent interaction.

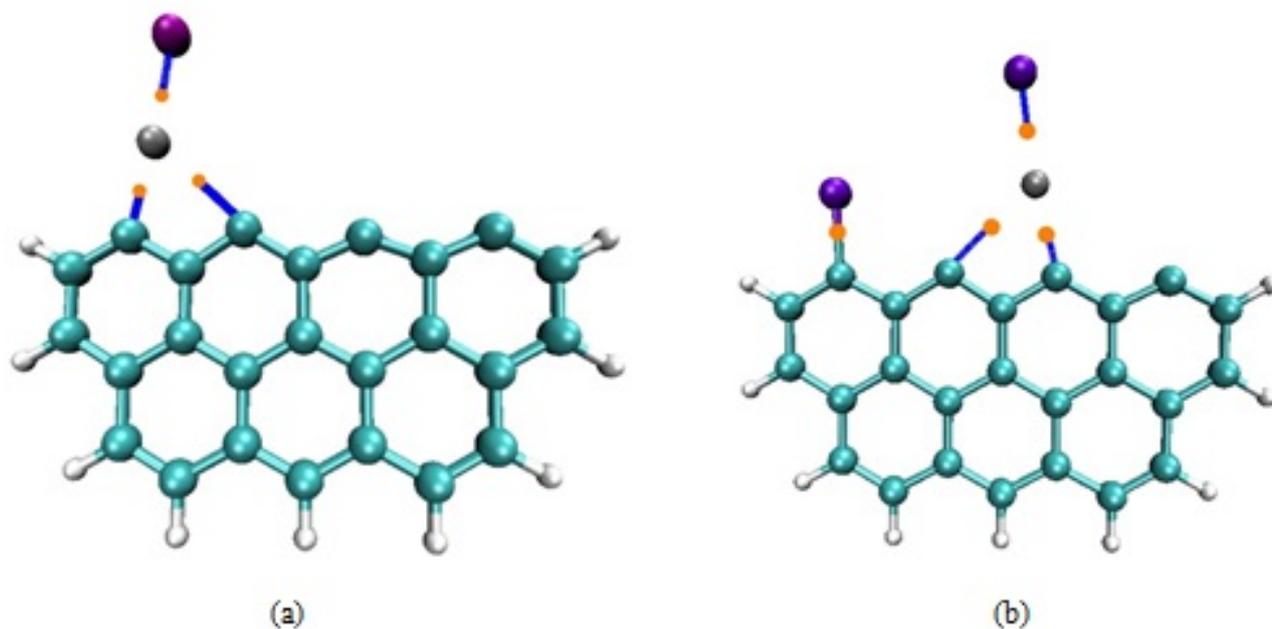


Fig. (7). Electron density topologies for (a) $\text{HgBr-C}_{25}\text{H}_9$ complex, (b) $\text{HgBr}_2\text{-C}_{25}\text{H}_9$ complex. Bond critical points (BCP) are shown in orange, paths are shown in blue.

Table 4. Topological parameters of the BCP of bond in adsorption configurations.

Configurations	Bond	ρ	$\nabla^2\rho$	G	V	H
$\text{C}_{25}\text{H}_9\text{-HgBr}$	Hg-Br	0.0811	0.1492	0.0595	-0.0818	-0.0222
	Hg-C ₁	0.0282	0.8266	0.0206	-0.0210	-0.0004
	Hg-C ₂	0.1161	0.1590	0.0862	-0.1326	-0.0464

Configurations	Bond	ρ	$\nabla^2 \rho$	G	V	H
C ₂₅ H ₉ -HgBr ₂	Hg-Br	0.0812	0.1486	0.0595	-0.0819	-0.0224
	Hg-C ₁	0.1138	0.1706	0.0870	-0.1313	-0.0443
	Hg-C ₂	0.0311	0.0893	0.0229	-0.0235	-0.0006
	Br-C	0.1676	-0.1903	0.0578	-0.1632	-0.1054

CONCLUSION

In one 4×300 MW coal-fired power plant, addition experiment and DFT theoretical calculation were conducted to study the effect of the CaBr₂ additive on mercury speciation at SCR entrance and export. Total gaseous mercury concentration through SCR increases due to the CaBr₂ addition, which may be the reason for HgBr oxidation and desorption under hydrogen halide condition. There is a saturation value of CaBr₂ addition, which makes the mercury oxidation behavior no longer enhanced. An overall effect indicates that CaBr₂ addition contribute to Hg²⁺ increasing and Hg⁰ decreasing, demonstrating the positive effect of transformation of Hg⁰ to Hg²⁺. The desorption of Hg²⁺ by HBr and Br₂ reacting with CaO and Ca(OH)₂ which is produced from CaBr₂ in high temperature flue gas may also be applied to explain the increase of total gaseous mercury concentration. DFT calculation results show that the bonding of HgBr and HgBr₂ with active sites is indicative of covalent interaction, and the Br-C bond is stronger than Hg-C bond. Both HgBr and HgBr₂ can stably adsorb on the unburned carbon surface.

CONFLICT OF INTEREST

The authors declare no conflict of interest, financial or otherwise.

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