# Thermal Properties and Three-Phase Structure of *cis*-1,4-Polybutadiene

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**Abstract:** The thermal properties of *cis*-1,4-polybutadiene (*cis*-PBD) were investigated in dependence of content of *cis* units and of linearity of the main chain. *cis*-PBD grades containing a fraction of *cis*-segments ranging from 93 to 98 %, and with linear or branched chains, were analyzed. Upon isothermal crystallization from the melt at -26 °C for 1 h, followed by cooling to below the glass transition temperature, *cis*-PBD develops a three-phase structure, where the mobile amorphous phase is equal to 0.41, independently of chain structure, crystallinity ranges from 0.23 to 0.28, and the rigid amorphous fraction varies from 0.31 to 0.35. Up to three main endotherms can be evidenced by calorimetry at slow heating rate, depending on chain regularity. The multiple melting behavior was discussed on the basis of the three-phase structure, as well as of crystallization kinetics.

Keywords: cis-1,4-polybutadiene, calorimetry, multiple melting, crystallization, rigid amorphous fraction.

## **INTRODUCTION**

Polybutadiene with a large content of *cis*-1,4-units (*cis*-PBD) is one of the most common polymers produced by the modern synthetic rubber industry, being it widely used for the production of tires [1]. Polybutadiene also has a major application for the production of golf balls, as well as impact modifier for polystyrene and acrylonitrile-butadiene-styrene resin (ABS) [1].

*Cis*-1,4-polybutadiene is a semicrystalline polymer. Semicrystalline polymers are often described in terms of a two-phase structure, composed of amorphous and crystalline moieties, where the sum of the mass fraction of the amorphous  $(w_A)$  and the crystalline  $(w_C)$  parts is equal to 1:

$$w_c + w_a = 1 \tag{1}$$

However, polymer science literature suggests that the above equation is often incorrect, as it is now recognized that a fraction of the amorphous material in semi-crystalline polymers has a restrained molecular mobility. This portion, that does not contribute to the bulk glass transition, is known as "rigid amorphous fraction" (RAF) and seems to be located at the interface between the crystalline and the mobile amorphous phases [2-3]. During the last few years, various independent studies in the literature, employing different experimental techniques such as FT-IR spectroscopy, differential scanning calorimetry and X-ray scattering techniques showed that a three-phase model is more appropriate to describe the structure of semicrystalline polymers [4-8]. According to this model, equation (1) is transformed to the following:

$$w_{C} + w_{A} + w_{RA} = 1 \tag{2}$$

where  $w_{RA}$  is the mass fraction of the rigid amorphous part.

Recent analyses revealed that the three-phase model is needed to adequately describe a number of properties of semicrystalline polymers. For poly(1-butene) it was shown that for a detailed understanding of the mechanical behavior, it is necessary to account for the role played by all the three nanophases, not by the crystal and mobile amorphous parts only. The points of coupling between the amorphous and crystalline structures, that compose the rigid amorphous part, act as nanoscopic stress-transfer, with remarkable effects on mechanical properties of the material [9]. Similarly, the rigid amorphous content needs to be explicitly taken into account to describe the yield behavior and the loss of crystallinity of poly(ethylene terephthalate) (PET) in uniaxial compression, as demonstrated in Ref. [10] upon analysis of the relation between the mechanical properties and the nanostructure of PET. The RAF is of importance also in determination of the barrier properties of semicrystalline polymers. MAF and RAF have different oxygen solubility, as quantified for PET, which mainly arises from the different specific volume of the two fractions, a property that can permit to tailor the barrier properties of PET goods [10].

Some influence of the rigid amorphous fraction on polymer melting behavior has been suggested in the literature. For poly(phenylene oxide) it was shown that the physical state of the rigid amorphous fraction controls the onset of melting [11]. The small endotherm that is often seen a few degrees above the isothermal crystallization temperature was proven to contain contributions due to mobilization of the RAF for several semicrystalline polymers, like nylon 6, isotactic polystyrene and many others [12-17]. For poly(ethylene terephthalate) it was demonstrated that this small endotherm arises from devitrification of the RAF and partial melting, and that the two processes take place simultaneously, being largely coupled [16-17]. For cis-PBD we have recently shown that not only the first endotherm, as seen for other semicrystalline polymers, but the overall multiple melting behavior is affected by the physical state of the RAF [18].

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The above discussion points to the importance of quantitative description of semicrystalline polymers in terms of the three-phase structure, for a proper understanding of materials properties. The three-phase structure may be affected by specific features of the polymer chain, like stereoregularity or degree of branching. These features influence not only the three-phase composition, but the overall thermal properties of the material. Such a study is the topic of the present article, where an investigation of the effects of chain regularity on the thermal properties and the three-phase composition of *cis*-1,4-polybutadiene is detailed.

### **EXPERIMENTAL PART**

#### Materials

*cis*-1,4-polybutadiene samples with different microstructure were specifically synthesized for this study using neodymium-based catalytic systems. They were kindly provided by Polimeri Europa S.p.A. (Ravenna, Italy). The molecular characteristics of the analyzed grades are given in Table 1, which reports the weight-average  $(M_w)$  and number-average  $(M_n)$  molecular mass, the molecular mass distributions and information on linearity and degree of branching of the used materials. The various samples were identified by a notation code, shown in the first column of Table 1, on the basis of contents of *cis* units and branching.

# **Differential Scanning Calorimetry**

Thermal properties were measured with a Mettler DSC822<sup>e</sup> equipped with a liquid nitrogen cooling system. The instrument was calibrated in temperature with high purity standards (indium, naphthalene and cycloexane) and in energy with heat of fusion of indium. Dry nitrogen was used as purge gas at a rate of 50 ml/min. Each measurement was repeated three times to improve accuracy.

To investigate the overall kinetics of isothermal crystallization, PBD samples were heated from room temperature to 70 °C at a rate of 20 °C/min, equilibrated at 70 °C for 3 minutes, then cooled at 30 °C/min to the desired crystallization temperature ( $T_c$ ) where they were allowed to crystallize.

In order to set the structure for the analysis of melting behavior, each *cis*-PBD sample was maintained at 70 °C for 3 min, then cooled at -30 °C/min to the crystallization temperature  $T_c = -26$  °C, where it was allowed to crystallize for 1 h. After isothermal crystallization PBD was cooled at -10 °C/min to -130 °C, equilibrated at -130 °C for 3 min, then heated until complete melting using either a constant scanning rate, of either 1 or 10 °C/min, or a modulated temperature profile. The TMDSC program was designed using the Star<sup>e</sup> software of Mettler-Toledo, Inc. Non-isothermal TMDSC data were gained using a sawtooth oscillation with a temperature amplitude  $(A_T)$  of 0.2 °C, an underlining heating rate (q) of 1 °C/min and modulation periods (p) of 60, 90, and 120 s. From TMDSC measurements the reversing specific heat capacity  $(c_{p,rev})$  was derived from the ratio of the amplitudes of modulated heat flow rate  $(A_{\phi,n})$  and temperature  $(A_{T,n})$ , both approximated with Fourier series [19]:

$$c_{p,rev}(\omega,n,t) = \frac{A_{\Phi,n}(t)}{A_{T,n}(t)} \frac{K(\omega,n,t)}{mn\omega}$$
(3)

where *t* is the time, *n* the order of the harmonic,  $\omega$  the base modulation frequency ( $\omega=2\pi/p$ ), *m* the mass of the sample and *K*(*n*, $\omega$ ,*t*) the frequency-dependent calibration factor. The reversing specific heat capacity data reported in this contribution were obtained from the first harmonics of the Fourier series.

#### **Optical Microscopy**

Spherulite growth rates were estimated by optical microscopy, using a Zeiss polarizing microscope equipped with a Linkam TMHS 600 hot stage and a Linkam CS 196 unit for fast cooling with liquid nitrogen. Samples for optical microscopy analysis were prepared by casting a drop of a 2 % toluene solution onto a glass slide, followed by drying under vacuum. The radius of the growing crystals was monitored during solidification by taking photomicrographs at appropriate intervals of time, using a JVC TK-1085E Video Camera. Spherulite radii were measured with the software Image-Pro Plus 3.0. Dry nitrogen gas was purged throughout the hot stage during all measurements and thermal treatments.

The thermal treatments before isothermal crystallization were identical to those used in calorimetry, and again each measurement was repeated three times. Spherulite growth rates (G) data were obtained in isothermal conditions from the initial slope of the radius (r) vs. time (t) plots [20].

# **RESULTS AND DISCUSSION**

Fig. (1) illustrates the spherulite growth rates (G) of the various materials as function of the crystallization temperature. As expected, in the analyzed temperature range the rate of crystal growth decreases with temperature. The fastest crystallization rate is seen in the sample with linear structure, containing 98% of *cis* units. Overall, G increases with chain regularity, as faster transition rates are observed for the polymers that have higher stereospecificity. The introduction of units with different configuration leads to slower phase

 Table 1.
 Molecular Characteristics of the cis-1,4-Polybutadiene Grades Used

Code	cis %	Mw (kDa)	Mn (kDa)	Mw/Mn	Structure
98-li	98	437	148	2.95	Linear
97-sb	97	380	100	3.8	Slightly branched
95-al	95	326	136	2.4	Almost linear
94-sb	94	360	144	2.5	Slightly branched
93-hb	93	354	136	2.6	Highly branched

transition kinetics. For the analyzed compositions, the influence of chain linearity is also of importance, as very low rates of crystal growth are measured for the branched *cis*-PBD polymers containing less than 94 % of repeating segments in the *cis* configuration.



Fig. (1). Spherulite growth rate of *cis*-PBD as a function of temperature.

The overall crystallization rate of cis-PBD is presented in Fig. (2), that reports the data of half-time of crystallization ( $\tau_{1/2}$ ) as a function of temperature. Fig. (2) reveals that relatively fast crystallization rate is attained by the commercial grade containing 97 % of *cis* segments, and that no specific trend can be correlated with chain structure, as for all the other compositions the  $\tau_{1/2}$  values are very similar, close to the experimental error. Even the significant polydispersity of the various grades, that may result in segregation effects [21], has no significant influence on crystallization rate.



Fig. (2). Half-time of crystallization of cis-PBD as a function of temperature.

The data reported in Figs. (1-2) indicate a main influence of primary nucleation on crystallization kinetics of the analyzed *cis*-PBD grades. The overall crystallization rate is determined by superposition of the rates of crystal nucleation and growth. The process of crystallization of polymers from the melt starts with primary nucleation, then continues with crystal growth and secondary crystallization [21]. As demonstrated in Ref. [22], the analyzed *cis*-PBD grades contain different types and/or amounts of heterogeneities that are more or less active to initiate the phase transition, and this process predominates over the kinetics of crystal growth. Overall, this results in a lack of correlation of the overall crystallization rate with chain structure, as well as with polydispersity, seen in Fig. (2). The onset of phase transition is determined by the activity of the foreign particles present in each *cis*-PBD sample. These are responsible for an anticipated beginning of the transition, that then proceeds with a rate that is mostly affected by chain structure, quantified in Fig. (1).

As mentioned above, crystallization data are needed for a complete description of the thermal properties of the *cis*-PBD grades, being the material structure defined upon crystallization, that proceeds, for each sample, with the kinetics detailed in Figs. (1-2).

The melting behavior of cis-PBD is illustrated in Fig. (3) at two different heating rates, 1 and 10°C/min, for the linear grade with 98 % of cis units in the chain. Experimental specific heat capacity of 98-li cis-PBD, measured after isothermal crystallization at -26 °C for 1 h, followed by cooling to -130 °C, is compared in Fig. (3) with thermodynamic  $c_p$  values of fully solid and liquid cis-PBD, as taken from the ATHAS Data Bank [23]. The insert in the upper left corner of Fig. (3) presents an enlargements of the DSC traces of 98li cis-PBD in the glass transition region. The  $c_p$  curves start to deviate from the baseline  $c_p$  data of solid polybutadiene at around -120 - -115 °C, due to the onset of the glass transition  $(T_g)$ . The temperature range where  $T_g$  takes place is affected by heating rate, moving to higher temperatures with the increase of the scanning rate, as typical for devitrification [24]. Additional thermal events partly cover  $T_{\rm g}$  in this temperature range, better seen in the enlargement presented as insert in Fig. (3), and the overall heat capacity jump appears to be affected by the experimental conditions, hindering a quantitative analysis of the amorphous fraction that mobilizes at  $T_g$  by conventional DSC. In order to separate the various reversing and non-reversing thermal events occurring in the glass transition region, temperature-modulated calorimetry analyses were conducted.

The reversing  $c_p$  plots determined from the TMDSC experiments at the underlying heating rate of 1 °C/min and various frequencies of modulation are compared in Fig. (4) with the conventional DSC traces reported in Fig. (3). Below the glass transition region and above completion of melting, DSC and TMDSC experimental data well agree with thermodynamic  $c_p$  of solid and liquid PBD, respectively. In the melting range the DSC and TMDSC signals are comparable. Erroneous deconvolution of the modulated signal occurs frequently when transitions with high latent heats are analyzed in TMDSC with an underlying heating rate. If irreversible endotherms and exotherms overlap, as is often the case in the analysis of the melting of polymers, the reversing heat capacities may even give larger contributions than the total latent heat, as demonstrated in Ref. [25-26]. In the temperature region of  $T_{g}$ , a minor frequency-dependence of the reversing heat capacity can be observed. The transition ob-



Fig. (3). Experimental specific heat capacity of 98-li *cis*-PBD measured upon heating by conventional DSC at the indicated rates, after isothermal crystallization at -26 °C for 1 h and subsequent cooling to -130 °C. The specific heat capacity of the solid and liquid *cis*-PBD, shown as dashed lines, are taken from the ATHAS data bank [23]. The insert in the upper left corner is an enlargement of the plot in the glass transition area.

tained from the reversing  $c_p$  curves of the temperaturemodulated data (dynamic  $T_g$ ), is located at temperatures slightly higher than the thermal glass transition measured under linear heating. This discrepancy is caused by the differences in the frequencies of the TMDSC analyses with those related to the ordinary linear heating rates, the latter being generally lower [27-29]. At completion of  $T_g$ , the reversing  $c_p$  curves gained by non-isothermal TMDSC data at three different frequencies overlap, revealing the real extent of the transition, apart from non-reversing events that inhibit correct determination of glass transition parameters of *cis*-PBD by conventional DSC. The heat capacity jump determined from the reversing  $c_p$  plots accounts for a mobile amorphous content  $w_A$  of 0.41<sub>3</sub>.



Fig. (4). Specific heat capacity of 98-li *cis*-PBD after isothermal crystallization at -26 °C and subsequent cooling, as measured upon heating. The solid lines are the total heat capacity by conventional DSC at the indicated rates, the thin lines are the reversing specific heat capacity measured by TMDSC at 1 °C/min and at the indicated periods of modulation. The specific heat capacity of the solid and liquid *cis*-PBD, shown as dashed lines, are taken from the ATHAS data bank [23].

The thermal properties of a number of grades of *cis*-PBD are shown in Fig. (5), that reports the DSC traces after iso-thermal crystallization at  $-26^{\circ}$ C for 1 h followed by cooling to  $-130^{\circ}$ C. The DSC plots presented in Fig. (5) refer to a heating rate of 1 °C/min, which was selected for being low enough to permit a good separation of the multiple thermal events occurring in the melting region, as seen by comparison of the St-DSC traces of the 98-li polymer in Fig. (3), and at the same time sufficiently high to allow a good signal-tonoise ratio. The various thermograms display a glass transition centered around -108 °C overlapped by additional thermal events of endothermic nature, discussed above, and a complex melting behavior.



Fig. (5). Specific heat capacity of the various *cis*-PBD after isothermal crystallization at -26 °C and subsequent cooling, as measured during heating at 1 °C/min.

As probed in Figs. (3-4) for the 98-li grade, analysis by St-DSC does not permit to measure the heat capacity step at the glass transition, necessary to quantify the content of mobile amorphous phase of PBD, which can instead be accomplished by temperature-modulated calorimetry. A comparison of the reversing specific heat capacity of the discussed cis-PBD polymers, measured by TMDSC at the same period of modulation of p = 120 s, is illustrated in Fig. (6). The reversing  $c_p$  curves of the various samples mostly overlap from below the  $T_g$  of the MAF up to about -80 °C, with some slight differences seen only in the breadth of the glass transition event, then display large dissimilarities in the reversing melting behavior, which however is not quantitative when analyzed by TMDSC with a non-zero underlying heating rate. Most importantly, the reversing  $c_p$  curves evidence that the mobile amorphous fraction does not vary, within the experimental uncertainty, for the analyzed *cis*-PBDs after isothermal crystallization at -26°C for 1 h.

The crystal fraction is quantified by integration of St-DSC plots, using eq. (4) [30-31]:

$$c_{p}(T) = w_{c}(T)c_{p,c}(T) + w_{A}(T)c_{p,A}(T) - [h_{A}(T) - h_{c}(T)]\frac{dw_{c}(T)}{dT}$$
(4)

where  $c_p(T)$  is the measured specific heat capacity,  $c_{p,C}(T)$ and  $c_{p,A}(T)$  the thermodynamic values of the crystalline and mobile amorphous specific heat capacities and  $[h_A(T)-h_C(T)]$ the heat of fusion, all tabulated in the ATHAS Data Bank [6]. Results of this analysis are presented in Fig. (7), that illustrates the evolution of crystal fraction with temperature



Fig. (6). Specific heat capacity of the various *cis*-PBD after isothermal crystallization at -26 °C and subsequent cooling, as measured during modulated heating at 1 °C/min and p = 120 s.

during fusion of the various PBD grades. As suggested in Ref. [32-33], the initial crystalline weight fraction of the material can be approximated by the maximum in the  $w_C$  vs. temperature plot. The crystallinity values deduced from the data of Fig. (7) are reported in Table 2. Comparison with the amount of mobile amorphous phase quantified by the heat capacity step at the glass transition probes that a considerable rigid amorphous fraction  $(w_{RA})$  develops in the cis-1,4polybutadienes under the experimental conditions, which is also reported in Table 2. It needs to be underlined that the  $w_{RA}$  values of Table 2 are probably underestimated, due to the approximation in calculation of the crystal fraction of eq. (4), that neglects possible devitrification of the RAF in the melting range. No information on the kinetics of RAF devitrification can be provided by analysis of the reversing  $c_p$ plots shown in Fig. (3), that display a clear frequencydependence starting from about -80°C, when reversing and non-reversing latent heat exchanges overlap possible initial mobilization of the rigid amorphous fraction.



**Fig. (7).** Temperature dependence of the enthalpy-based crystallinity of *cis*-PBD during heating at 1 °C/min, calculated with eq.(4).

Fable 2.	Nanophases' Content of the cis-1,4-Polybutadiene						
	Grades Used after Isothermal Crystallization at -26						
	°C for 1 h Followed by Cooling to -130 °C						

Code	WA	w <sub>C</sub>	W <sub>AR</sub>
98-li	0.413	0.272	0.315
97-sb	0.413	0.277	0.310
95-al	0.413	0.249	0.338
94-sb	0.413	0.242	0.345
93-hb	0.413	0.235	0.352

The data shown in Table 2 reveal that no straightforward relation between chain microstructure and nanophase content can be derived for cis-PBD, as the effects of crystallization kinetics overlap with chain regularity. For a same thermal history (isothermal crystallization at -26 °C for 1 h followed by cooling to -130 °C), the analyzed polymers develop the same amount of mobile amorphous fraction. Crystallinity roughly increases with chain regularity, as the grades with a low cis fraction display low levels of crystallinity. Crystallization rate also affects composition of the 3-phase structure, since the 97-sb grade, that has the fastest transition kinetics, probably due to the presence of nucleating agents in the formulations, is the polymer that develops the largest crystal fraction. This in turn, corresponds to a low RAF. Crystallization of PBD at -26 °C is completed in 8 - 25 min, depending on the grade. The time of residence at -26 °C was extended for all the samples to 1 h, in order to provide exactly the same thermal treatment for all the polymers. This corresponds to a longer time available for crystal perfection following primary crystallization to the grades that crystallize faster. The structural rearrangements following primary crystallization allow development of a larger crystal fraction, which in turn results in a reduction of the strained amorphous portions coupled with the perfected material. It is interesting to note that this process involves only the crystalrigid amorphous interface, with no influence of the bulk amorphous phase that attains the same level in all the analyzed polymers.

As mentioned above, the multiple melting behavior of cis-PBD is illustrated in Fig. (5). All the analyzed grades display a small endotherm centered at -23°C, i.e. 3°C above the temperature of isothermal crystallization. This small DSC peak, that appears in a number of semicrystalline polymers a few degrees above the crystallization temperature, arises from the simultaneous occurrence of partial fusion of the crystals and enthalpy recovery connected to structural relaxation of part of the rigid amorphous fraction, as also discussed in the Introduction Section [16-17]. Neither the specific chain regularity, nor the three-phase composition seem to affect this small thermal event, at least for the analyzed cis-PBD grades. Conversely, large differences in the major melting peaks are displayed by the various samples. The PBD grades with a large content of cis units have melting endotherms centered at -9 and -3 °C. When cis content decreases below 95 %, the two endotherms merge in a single peak, with a small shoulder appearing in the high temperature side of the peak in the samples with 94 and 95% cis segments. No shoulder is instead detectable in the major melting peak of the 93-hb *cis*-PBD grade, which has not only the smallest *cis* units percentage in the chain, but also a highly branched structure. This specific polymer has also a low crystallization rate, as quantified in Figs. (1 and 2).

In Ref. [18] it was shown that devitrification of the rigid amorphous fraction overlaps fusion in *cis*-PBD. Not only the first endotherm, as seen for other semicrystalline polymers, but the overall multiple melting behavior is affected by the physical state of the RAF. The multiple endotherms seen in the DSC plots of cis-PBD arise from partial melting and recrystallization. Upon heating, the strained amorphous segments start to mobilize, allowing the onset of melting of the crystals that have reached the upper limit of their thermal stability, and can subsequently develop more stable structures. To allow development of perfected crystals with improved thermal stability in the temperature range of the second major endotherm it is necessary that rigid amorphous fraction attains sufficient mobility. Two distinct major melting peaks are seen only in the PBD grades with high *cis* content that develop considerable crystallinity, and lower degree of RAF. These two polymers also display a large crystal fraction, compared to the other samples, and the crystal fraction develops at the expense of the RAF. It is possible that the rigid amorphous fraction in the grades with 97 % and more of cis segments is more strained than in the other PBD polymers, and the high degree of coupling between the rigid amorphous fraction and the crystal phase in PBD results in multiple melting appearance of the DSC traces. However, this is just a hypothesis, as the multiple melting seen in the grades with at least 97 % cis units may arise from the higher degree of perfection of the crystallites, together with a faster recrystallization kinetics, that facilitate partial melting followed by recrystallization into thickened and less defective crystallites during the DSC scan at 1 °C/min. Conversely, in the cis-PBD polymers with a less regular chain partial melting is followed by very limited recrystallization, that does not result in a separate endothermic peak, but only as a small shoulder in the DSC trace.

## CONCLUSIONS

Conventional and temperature-modulated DSC analyses allowed to quantify the influence of chain microstructure on thermal properties of *cis*-PBD. All the analyzed grades develop, upon isothermal crystallization from the melt followed by cooling, a three-phase structure, whose composition depends on the specific features of the polymer chain, as well as on crystallization kinetics. All the analyzed grades have the same amount of mobile amorphous phase, whereas dissimilarities exist in crystallinity level and rigid amorphous content.

Similarly to other semicrystalline polymers, *cis*-PBD displays a small endotherm a few degrees above the isothermal crystallization temperature. This thermal event, that is caused by concurrent partial melting of the crystal phase and partial devitrification of the rigid amorphous fraction, is independent of chain structure and composition. Additional endotherms are also present at higher temperatures. The polybutadienes with a high *cis* content show two separate endothermic events at high temperatures, caused by partial melting and recrystallization, which overlap with full mobi-

lization of the rigid amorphous fraction. In the grades with lower degree of chain regularity, the two endotherms merge into a single peak, at least under the used experimental conditions, as the partial melting-recrystallization processes take place to a more limited extent.

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